

**LIMITED SUBSURFACE SOIL EXPLORATION AND
PRELIMINARY GEOTECHNICAL ENGINEERING EVALUATION
606-ACRE PROPERTY - WARFIELD BOULEVARD (SR-710)
PHASE 1 - PROPOSED DATA PROCESSING CENTER
INDIANTOWN, MARTIN COUNTY, FLORIDA**

AACE FILE NO. 25-235



ANDERSEN ANDRE CONSULTING ENGINEERS, INC.

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Silver Fox 606, LLC
12800 US Highway One, Suite 300
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Attention: Mr. Nelson Ferreira

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1.0 INTRODUCTION

In accordance with your request and authorization, Andersen Andre Consulting Engineers, Inc. (AAACE) has completed a limited subsurface exploration and preliminary geotechnical engineering analyses for the above referenced project. The purpose of performing this evaluation was to preliminarily explore shallow soil types and groundwater levels in order to provide introductory Geotechnical Engineering recommendations for the development of the subject property. Our work included Standard Penetration Test (SPT) borings, hand auger borings, soil hydraulic conductivity (exfiltration) testing, piezometer installation, laboratory testing, and engineering analysis.

This report documents our explorations and presents our findings, and summarizes our preliminary opinions. We note that additional subsurface soil explorations will need to be performed once the final locations and details of the proposed development features have been determined. Complete recommendations for site preparation procedures and foundation design for the individual project components can be provided once these additional exploratory efforts have been completed.

1.1 Site Location and Description

The overall subject site consists of the following two adjacent properties located near the southwest corner of SW Warfield Bouelvard (SR-710) and Silver Fox Lane in Indiantown, Martin County, Florida (within Sections 27 & 34, Township 39 South, Range 38 East):

- Parcel ID 27-39-38-000-00040-3 (322.38 acres)
- Parcel ID 34-39-38-000-00011-4 (280.40 acres)

A Site Vicinity Map (2025 aerial photograph) which depicts the location of the site is included on the attached Figure No. 1. The site location is further shown superimposed on the “Barley Barber Swamp, Florida” USGS topographic quadrangle map, also included on Figure No. 1. The USGS map depicts the subject site as being undeveloped and relatively level with an approximate surface elevations of 30 to 35 feet relative to the National Geodetic Vertical Datum of 1929.

The overall 600+ acre site is currently heavily wooded and has numerous wetlands that cover more than one-third of the site. The Phase 1 area (the subject of this report) where the Data Processing Center campus is proposed is accessible via trails and open areas that includes a ±50-acre area where overgrown rows of composting material are located. Additional site features include cattle fencing, a ±7-acre lake, drainage ditches and a ±3,600SF metal maintenance building.

1.2 Aerial Photograph Review

Our review of historical aerial photographs compiled during our previously completed Phase 1 Environmental Site Assessment report for this site (refer to AACE File No. 25-129, report dated March 26, 2025) indicate that the site was idle/vacant from around 1940 to about 1980. In 1980 an FPL power line easement had been cleared within the northern one-third of the site. The site conditions then remained relatively unchanged until around 2004 when a composting operation can be seen. This composting operation was active until around 2015 where the rows of composting material appear to be overgrown, indicating that the composting operation had ceased. The site appears to be unchanged from 2015 until present day.

1.3 Project Description

Based on our conversations with representatives of the project Civil Engineering firm (LaConte Engineering), and our review of the provided site plan (dated November 6, 2025), we understand that Phase 1 of the overall industrial development of the site will consist of a data processing center campus, which will include several two-story buildings along with infrastructure improvements. The final locations of the proposed buildings have not been determined at this point in time, however, a general area for Phase 1 has been selected. While we have not been provided with any specific structural loading information for the proposed buildings, we expect that they will have maximum wall loads of 8-10 kips per lineal foot and maximum column loads of 250 kips.

We further understand that, at this point, only limited subsurface soil and groundwater level information (including normal seasonal high groundwater table estimates) is being requested, with the understanding that a design-level geotechnical study should be performed prior to finalizing construction drawings.

Should our understanding of the future site development differ significantly from what is described above, we request that we be contacted and given the opportunity to review proposed development plans as they relate to the opinions and recommendations presented herein.

2.0 LIMITED FIELD EXPLORATION PROGRAM

Subsurface conditions were explored through a review of the U.S. Department of Agriculture (USDA) Web Soil Survey, through site reconnaissance, and by the performance of soil borings and soil hydraulic conductivity tests. The purposes of the exploration were (1) to investigate subsurface conditions (i.e. soil types, groundwater levels, etc.) at the subject site, (2) to preliminarily obtain a measure of pertinent engineering properties of subsurface materials and (3) to present restrictions (if any) which these soil and groundwater conditions may place on future site development.

2.1 Review of USDA Soil Survey

Based on our review of the USDA NRCS Web Soil Survey, the Phase 1 site is generally located in an area characterized by the following shallow soil types:

- Lawnwood and Myakka fine sands (USDA NRCS Map Unit 2)
Sandy marine deposits originating from within marine terraces on flatwoods, with fine sands and loamy fine sands present to depths in excess of 80 inches below grade.
Drainage Class: Poorly drained. Depth to water table: About 6 to 18 inches.
- Waveland and Immokalee fine sands (USDA NRCS Map Unit 4)
Sandy marine deposits originating from within flatwoods on marine terraces, with fine sands and loamy fine sands present to depths in excess of 80 inches below grade.
Drainage Class: Poorly drained. Depth to water table: About 6 to 18 inches.
- Placid and Basinger fine sands, depressional (USDA NRCS Map Unit 13)
Sandy marine deposits originating from within depressions on marine terraces, with fine sands present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches
- Wabasso sand (USDA NRCS Map Unit 17)
Sandy and loamy marine deposits originating from within flatwoods on marine terraces, with fine sands, sandy clay loam and loamy sand present to depths in excess of 80 inches below grade.
Drainage Class: Poorly drained. Depth to water table: About 6 to 18 inches
- Floridana fine sand, frequently ponded, 0 to 1 percent slopes (USDA NRCS Map Unit 38)
Sandy and loamy marine deposits originating from within depressions on marine terraces, with fine sands and fine sandy loam present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches

- Cypress Lake fine sand, 0 to 2 percent slopes (USDA NRCS Map Unit 44)
Sandy and loamy marine deposits over limestone over sandy marine deposits, with fine sands, fine sandy loam and bedrock present to depths in excess of 80 inches below grade.
Drainage Class: Poorly drained. Depth to water table: About 6 to 18 inches
- Jupiter sand (USDA NRCS Map Unit 48)
Sandy marine deposits over limestone originating from within flats on marine terraces, with sands, bedrock, sandy clay loam and sandy loam/loamy sand present to depths in excess of 80 inches below grade.
Drainage Class: Poorly drained. Depth to water table: About 6 to 18 inches
- Riviera fine sand, frequently ponded, 0 to 1 percent slopes (USDA NRCS Map Unit 49)
Sandy and loamy marine deposits originating from within depressions on marine terraces, with fine sands and fine sandy loam present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches
- Chobee muck, 0 to 1 percent slopes (USDA NRCS Map Unit 57)
Loamy alluvium originating from within depressions on marine terraces, with muck, loamy sands, sandy loam, sandy clay loam and fine sands present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches
- Gator and Tequesta muck (USDA NRCS Map Unit 58)
Herbaceous organic material over loamy and sandy marine deposits originating from within depressions on marine terraces, with muck, sandy loam and fine sands present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches
- Samsula muck, frequently ponded, 0 to 1 percent slopes (USDA NRCS Map Unit 73)
Herbaceous organic material over sandy marine deposits originating from within depressions on marine terraces, with muck and sands present to depths in excess of 80 inches below grade.
Drainage Class: Very poorly drained. Depth to water table: About 0 inches

The approximate location of the site is shown superimposed on a copy of the USDA NRCS Web Soil Survey aerial photograph on Figure No. 2. Further, excerpts from the USDA NRCS Web Soil Survey summary report are included in Appendix I.

We note that the three soil types that are noted to include surface muck/organics (Map Units 57, 58 and 73) are located in small pockets outside of where the proposed data center building area is shown on the provided site plan. Further, the two soil types that are noted to have shallow “bedrock” conditions (Map Units 44 and 48) are located within the very southern portion of the site, outside of the proposed building areas.

2.2 Field Work

To preliminarily explore subsurface conditions at the site, the exploration program summarized in Table 1 below was completed:

Table 1 - Field Exploration Program

Field Work Type	Standard	# of Borings/Tests	Depth Below Grade [feet]	Location
Standard Penetration Test (SPT)	ASTM D1586	6	50	Refer to Figure No. 3
Hand Auger	ASTM D1452	10	4 - 6	Refer to Figure No. 3
Soil Hydraulic Conductivity Test	SFWMD ERPIM ⁽¹⁾	3	6	Refer to Figure No. 3
Piezometer Installations	NA	3	7	Refer to Figure No. 3

Note to Table 1: (1) SFWMD Environmental Resource Permit Information Manual

Our site visits and field exploration program were completed in the period November 24 through December 10, 2025. The field work locations shown on Figure No. 3 were determined in the field by our field crew using the provided site plan, aerial photographs, existing site features and a hand-held GPS unit. The locations should be considered accurate only to the degree implied by the method of measurement used. We preliminarily anticipate that the actual locations are within 15 feet of those shown on Figure No. 3.

Summaries of AACE's field procedures are presented in Appendix II and the individual boring profiles are presented on the attached Sheets No. 1-3. Samples obtained during performance of the borings were visually classified in the field, and representative portions of the samples were transported to our laboratory in sealed sample jars for further classification. The soil samples recovered from our explorations will be kept in our laboratory for 60 days, then discarded unless you specifically request otherwise.

3.0 LABORATORY TESTING PROGRAM

Our drillers observed the soil recovered from the SPT sampler and augers, placed the recovered soil samples in moisture-proof containers, and maintained a log for each boring. The recovered soil samples, along with the field boring logs, were transported to our Port St. Lucie soils laboratory where they were visually examined by AACE's project engineer to determine their engineering classification. The visual classification of the samples was performed in general accordance with the Unified Soil Classification System, USCS. Further, representative samples were selected for limited soil index property laboratory testing, consisting of moisture content tests (ASTM D2216) and percent fines tests (ASTM D1140). These tests were performed to aid in classifying the soils and to help evaluate the general engineering characteristics of the site soils. The results of our visual classifications and laboratory analyses are presented on the soil boring profiles on Sheets No. 1-3.

4.0 GENERAL SUBSURFACE SOIL AND GROUNDWATER CONDITIONS

4.1 General Soil Profile

Detailed subsurface conditions are illustrated on the soil boring profiles presented on Sheets No. 1-3. The stratification of the boring profiles represents our interpretation of the field boring logs and the results of laboratory examinations of the recovered samples. The stratification lines represent the approximate boundary between soil types. The actual transitions may be more gradual than implied.

In general, at the locations and depths explored, our borings encountered a thin mantle of topsoil (sands with roots/organics), followed by loose to dense fine sands (SP), fine sands with hardpan (SP, hardpan-type), slightly clayey fine sands (SP-SC) and clayey fine sands (SC) to depths of about 24 to 29 feet. At this depth a dense to very dense stratum of cemented sands and shell (L) was encountered to depths of about 34 to 43 feet, in turn followed by medium dense to very dense fine sands (SP) and slightly silty fine sands (SP-SM) reaching the termination depths of our borings.

The above soil profile is outlined in general terms only; please refer to Sheets No. 1-3 for individual soil profile details.

4.2 Measured Groundwater Level

The groundwater table depth as encountered in the borings during the field investigations is shown adjacent to the soil profiles on the attached Sheets No. 1-3. As can be seen, at the time of our field work, the groundwater table was encountered at depths ranging from approximately 2 to 4 feet below the existing ground surface, with this range likely due to similar variations in site topography. Fluctuations in groundwater levels should be anticipated throughout the year primarily due to seasonal variations in rainfall and other factors that may vary from the time the borings were conducted.

The stabilized groundwater table depths were measured within the installed ± 7 -ft deep piezometers on two occasions during the months of November and December, 2025 (Table 2):

Table 2 - Piezometer Groundwater Table Measurements

Piezometer ID	Groundwater Depths (ft-bls)	
	11/25/25	12/08/25
PZ-1	2.1	2.5
PZ-2	2.3	2.4
PZ-3	3.1	3.2

4.3 Estimated Normal Seasonal High Groundwater Table

In general, the normal seasonal high groundwater table (NSHGWT) is likely during (or in the latter part of) the rainy season in South Florida, which typically ranges from June through September/October of each year. The water table elevations associated with a 100-year flood level (or during an extreme storm event) would be much higher than the normal seasonal high water table elevation. The normal seasonal high groundwater table can also be influenced by the presence of relief points such as canals, lakes, ponds, swamps, etc., as well as by the drainage characteristics of the in-situ soils.

Based upon our field explorations and laboratory examinations, measurements of the ambient groundwater levels, our review of the USDA soil survey, and considering the time of year when our explorations were performed, we estimate that the NSHGWT is about 2 feet above the levels measured in the piezometers (Table 2).

Note that the estimated NSHGWT elevation does not provide any assurance that the groundwater levels will not exceed these estimated levels during any given year in the future. Drainage impediments, storm events or other such occurrences may result in groundwater levels exceeding our estimates. If a more accurate determination of the seasonal groundwater level variations on this site is prudent for the design of the project, we would recommend installing piezometers to allow for a prolonged period of groundwater monitoring.

4.4 Soil Hydraulic Conductivity Testing

Three (3) soil hydraulic conductivity tests were performed at the approximate locations shown on Figure No. 3. In general, the tests were performed in substantial accordance with methods described in the South Florida Water Management District (SFWMD) Environmental Resource Permit Information Manual (ERPIM) and yielded the following results (Table 3 and Appendix III).

Table 3 - Soil Hydraulic Conductivity Test Results

Test No.	Groundwater Depth (ft-bls)	Flow Rate, Q (cfs)	Hydraulic Conductivity, K (cfs/sqf - ft head)
EX-1	2	2.0×10^{-4}	1.2×10^{-5}
EX-2	3	4.5×10^{-3}	2.0×10^{-4}
EX-3	2	3.3×10^{-3}	2.1×10^{-4}

5.0 PRELIMINARY GEOTECHNICAL ENGINEERING EVALUATION

5.1 General

The following preliminary evaluation is based on a review of the attached soil boring profiles, our understanding of the project and its current status, and on our experience with similar projects and subsurface conditions. Once plans for development of the subject site have been finalized, the preliminary evaluation presented herein should be supplemented with additional field explorations designed specifically for the proposed construction.

5.2 Structures

In summary, it is our preliminary opinion that the soils on this site are generally adequate to support future low-rise building construction on conventional shallow foundations following typical site preparation methods.

Overall, future site preparation procedures for this site will include clearing of the vegetation currently present on the site (making sure to fully remove stumps, composting materials, etc.), backfilling of craters/excavations from such features, leveling of uneven terrain, and proofrolling of the building and pavement areas with heavy vibratory compaction equipment. Further, the existing drainage ditches should be dewatered, cleaned and reclaimed with granular fill placed in thin, individually compacted lifts.

Once the site has been properly prepared, conventional shallow foundations or monolithic slabs proportioned for an allowable soil bearing pressure of 2,500 pounds per square foot (psf) can be used for support the proposed building construction.

Should the project require higher allowable soil bearing pressures, the foundation soils for the proposed buildings can be improved using the Vibro-Replacement Technique (VRT) to depths of about 30-35 feet below the foundation bearing level (i.e. to the top of the encountered dense to very dense cemented sand and shell stratum). VRT is a deep foundation improvement method typically used to densify loose strata of mixed silt-clay/sand soil matrices. It is performed by inserting a vibratory probe into the ground under its own weight as water is injected through the probe tip. Loose sands around the vibrating probe liquefies and is displaced laterally. The excess water is expelled at the ground surface and clean gravel (FDOT #57 stone) is added to the formed depression to maintain the desired ground elevation and to fill the space occupied by the probe as it is retrieved. The result is a column of densified sand and gravel ("stone columns") with a diameter of 5 to 6 feet. Shallow foundations supported on soils improved with VRT can be proportioned for a maximum allowable bearing pressure of 5,000 psf.

5.3 Pavements

The results of our preliminary exploration indicate that the subject site, if prepared properly, is typically suitable for supporting parking/drive areas using a conventional flexible pavement section with an asphaltic concrete wearing surface, a calcareous base course, and compacted, stabilized subgrade. Site preparation is anticipated to consist of the removal of organic topsoil (where encountered) and densification of near-surface soils by compacting the cleared and grubbed ground surface with conventional compaction equipment prior to the placement of embankment soils and/or pavement.

In order to reduce the potential for premature roadway distress, including base deterioration or failure, a minimum separation of 18 inches should be maintained between the estimated normal seasonal high groundwater level and the bottom of the limerock/coquina pavement base course. If this is not possible, the use of an asphaltic "black-base" (i.e. FDOT Type B-12.5) or the installation of roadway edge underdrains may be required.

5.4 Retention Ponds and Use of Fill Soils (Borrow Suitability)

Based on the results of our preliminary exploration, it is not anticipated that heavy duty excavation equipment will be required to excavate soil from within stormwater ponds or utility/drainage installations within depths of about 30 feet below grade. Conversely, should any proposed stormwater ponds be designed to be deeper than about 30 feet below grade, it should be anticipated that the encountered dense to very dense cemented sand and shell stratum will be difficult to excavate.

Based on visual examination of the recovered soil samples, and on our experience from numerous similar construction projects Martin County, we offer the following general comments with regards to the suitability of the encountered soils for use as structural fill materials:

- Fine sands (SP) should be suitable to serve as fill soils and with proper moisture control should densify using conventional compaction equipment. Soils obtained from below the water table may require time to dry sufficiently. However, these materials should be suitable for relatively unrestricted use as fill and embankment.
- Slightly clayey fine sands (SP-SC) and slightly silty fine sands (SP-SM) with fines contents less than 10-15 percent are suitable for structural fill, but will likely be more difficult to compact due to their inherent nature to retain excess soil moisture. If the use of slightly clayey soils is desired, it may be necessary to stockpile these soils in order for them to drain. Thinner lifts (perhaps 6 to 8 inches in loose thickness) may be required for placement and compaction of these soils. Further, it may become necessary to mix these soils with drier, cleaner granular sands prior to placement to increase the "workability" of these soils.

- Clayey fine sands (SC) with fines content in excess of 15-20 percent are generally considered undesirable for use as structural fill because of the difficulty in conditioning and working the material due to its high fines content. However, clayey soils can possibly be mixed with sands with less fines content (i.e. less than 5 percent passing the U.S. No. 200 sieve) and likely be used provided that the post-mixing fines content is not greater than 10 percent.
- Organic topsoil is not considered suitable for use as any type of fill, other than in landscaped areas or other non-structural areas.

We note that most of our borings encountered a thin, near-surface layer of dark brown/brown fine sands which included silt and hardpan fragments, a soil type that is locally known as hardpan-type soils. This hardpan stratum may be significantly more cemented and hard in areas not explored. While hardpan is generally suitable for use as a fill material, hardpan-type soils can be challenging for several reasons:

- Hardpan can be difficult to excavate, often requiring special equipment, especially in confined excavations such as utility or drainage trenches/excavations.
- Excavated hardpan-type soils are often boulder-size chunks of cemented soils which are not easily broken down for re-use as structural fill.
- When pulverized into fragments that can be compacted to an adequately dense matrix, the in-place soil often fails the relative compaction test because during laboratory preparation, the soil is pulverized into smaller particles, resulting in a denser laboratory matrix than that which occurs in the field.
- Alternative acceptance criteria may need to be implemented for hardpan-type soils used as fill. This criteria would need to be developed on a site specific basis after observing the contractor's earthwork methodology and the nature and condition of the compacted hardpan-type soils.

With respect to stormwater ponds or retention/detention areas, the hardpan-type soils are often relatively impervious and typically create a horizontal groundwater flow until a fracture in the hardpan occurs. Consideration can be given to overexcavating such hardpan-type soils from within the ponds or retention/detention areas so as to facilitate a more rapid drainage, if needed. Backfill in the detention or retention areas should consist of free-draining sandy materials with fines content less than 4 percent by dry weight passing the U.S. No. 200 sieve. The backfill should be placed in level lifts of 12-18 inches and receive some measure of compaction which likely can be accomplished by overlapping travel paths of loaded earthmoving equipment. The depth of this overexcavation will be dependent upon the pond design.

6.0 CLOSURE

The preliminary geotechnical evaluation submitted herein is based on the data obtained from the soil borings presented on Sheets No. 1-3, our understanding of the proposed project and its current status, and the assumed loading conditions previously described. Should the proposed site development differ significantly from what is described herein we request that we be notified to ensure that the preliminary recommendations presented herein are valid for the project. Additional limitations and conditions to this report are presented in Appendix IV.

This report includes the recommendation to perform additional exploratory borings within future development areas prior to completing project plans and specifications. Specific and design-level geotechnical engineering recommendations for site preparation, grading, foundation design, pavement construction, etc. can be provided following these additional explorations.

This report has been prepared in accordance with generally accepted soil and foundation engineering practices for the exclusive use of Silver Fox 606, LLC for the proposed subject project. No other warranty, expressed or implied, is made.

We are pleased to be of assistance to you on this phase of your project. When we may be of further service to you or should you have any questions, please contact us.

Sincerely,
ANDERSEN ANDRE CONSULTING ENGINEERS, INC.



Peter G. Andersen, P.E.
Principal Engineer
Fla. Reg. No. 57956



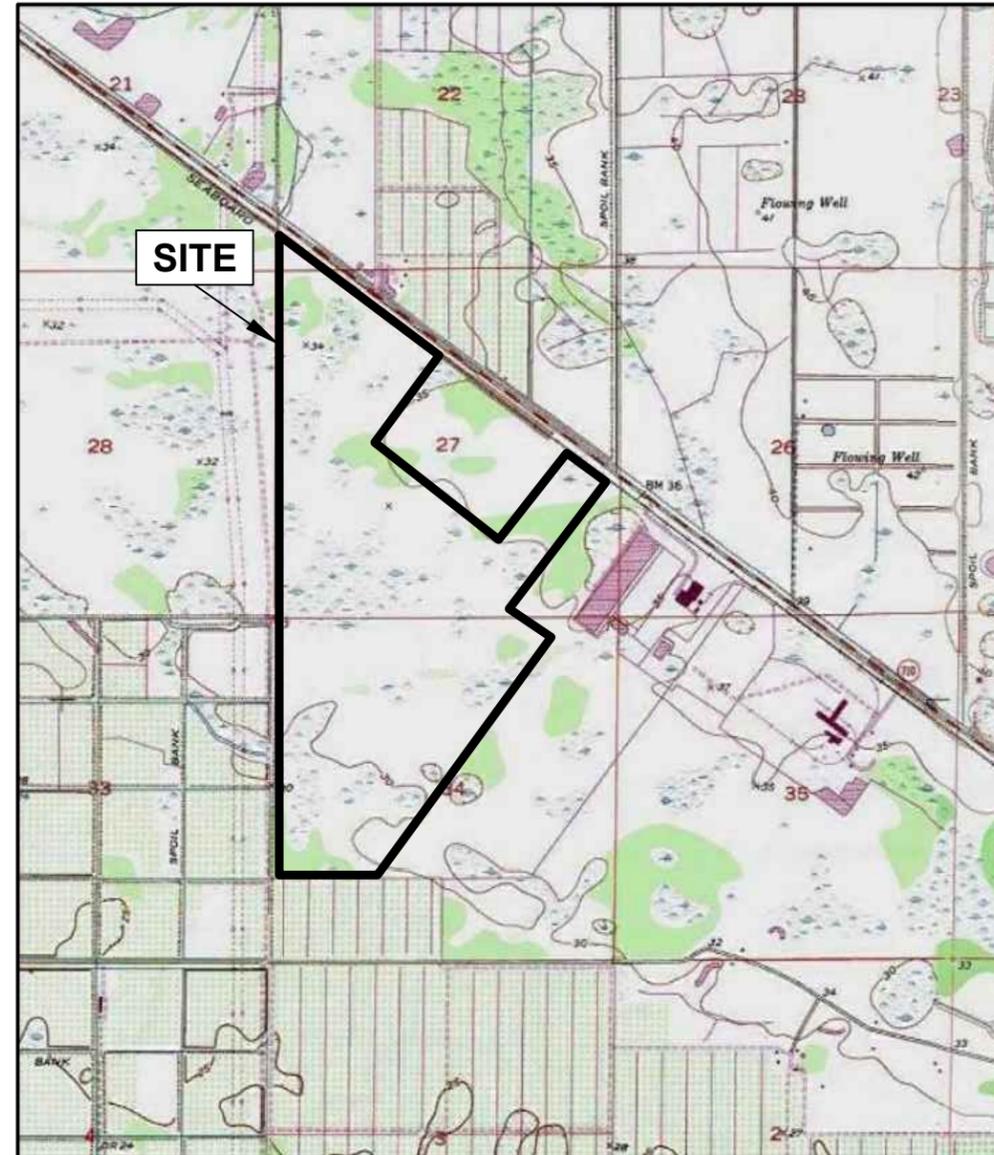
David P. Andre, P.E.
Principal Engineer
Fla. Reg. No. 53969

This report has been digitally signed by Peter G. Andersen, P.E. on the date adjacent to the seal. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

2025 AERIAL PHOTOGRAPH



USGS TOPOGRAPHIC QUADRANGLE MAP OF "BARLEY BARBER SWAMP, FL"



PUBLIC LAND SURVEY SYSTEM

Sections 27 & 34, Township 39 South, Range 38 East

NOT TO SCALE

Sources:
 - Google Earth Pro
 - QUADS/Earth Survey

MARTIN COUNTY PROPERTY APPRAISER

Parcel ID 27-39-38-000-000-00040-3 (322.38 acres)
 Parcel ID 34-39-38-000-000-00011-4 (280.4 acres)
 Parcel ID 22-39-38-000-000-00040-4 (3.7 acres)



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SITE VICINITY MAPS

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Drawn by: PGA

Checked by: DPA

AACE File No: 25-235

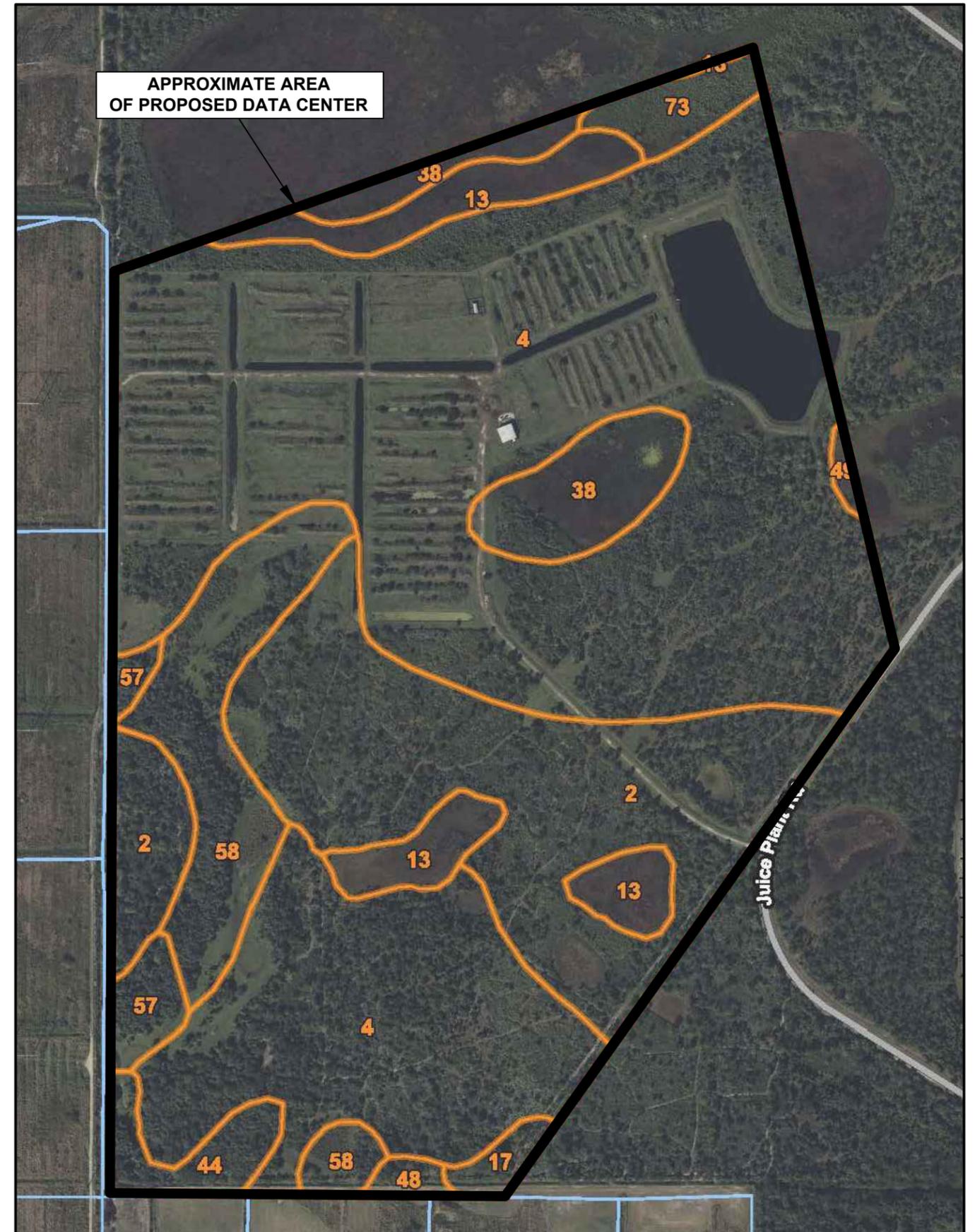
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Date: December 2025

Figure No. 1

USDA NRCS SOIL TYPES WITHIN SITE

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
2	Lawnwood and Myakka fine sands	49.4	19.0%
4	Waveland and Immokalee fine sands	154.5	59.4%
13	Placid and Basinger fine sands, depressional	12.4	4.8%
17	Wabasso sand, 0 to 2 percent slopes	1.7	0.6%
38	Floridana fine sand, frequently ponded, 0 to 1 percent slopes	10.7	4.1%
44	Cypress Lake fine sand, 0 to 2 percent slopes	4.3	1.6%
48	Jupiter sand	1.1	0.4%
49	Riviera fine sand, frequently ponded, 0 to 1 percent slopes	0.6	0.2%
57	Chobee muck, frequently ponded, 0 to 1 percent slopes	3.7	1.4%
58	Gator and Tequesta mucks	17.8	6.9%
73	Samsula muck, frequently ponded, 0 to 1 percent slopes	3.8	1.5%
Totals for Area of Interest		259.8	100.0%



NOT TO SCALE

Source:
- USDA NRCS Web Soil Survey



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USDA SOIL SURVEY MAP

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Drawn by: PGA

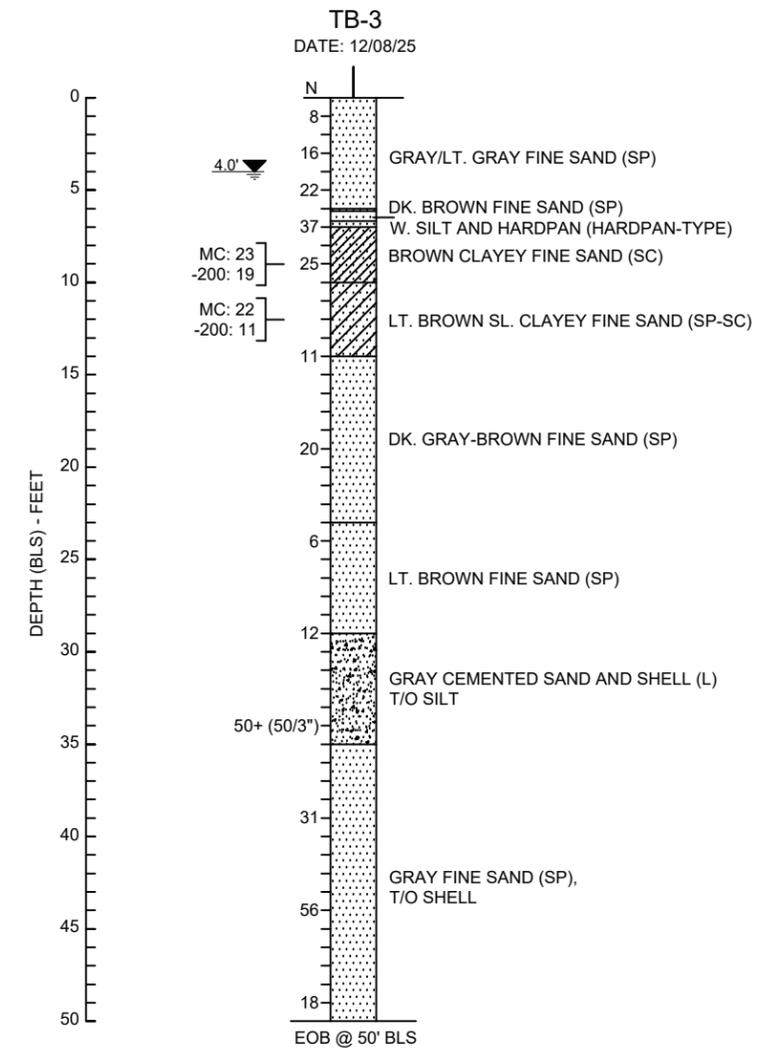
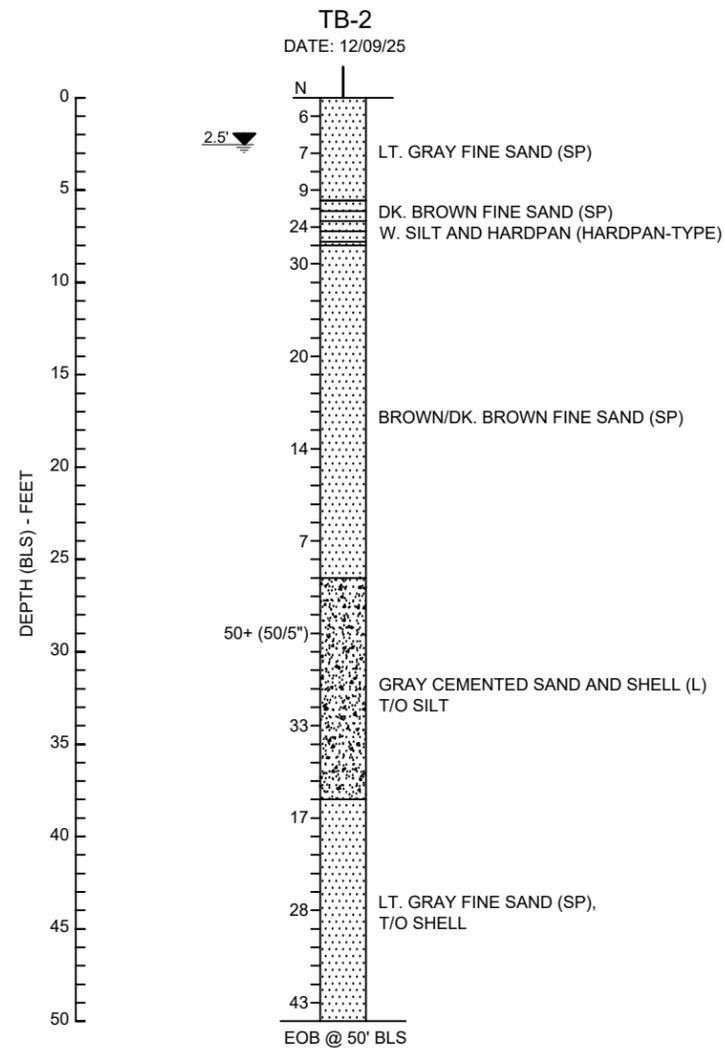
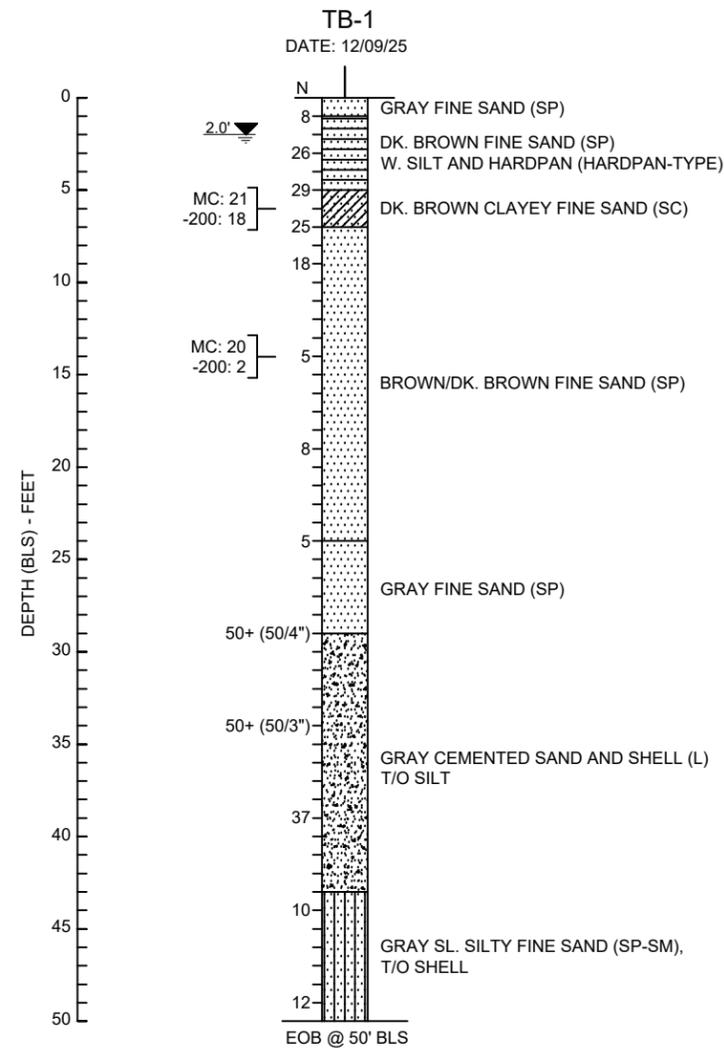
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Figure No. 2



SOIL GRAPHICAL LEGEND:

- FINE SAND (SP)
- FINE SAND (SP) W. SILT AND HARDPAN [HARDPAN-TYPE]
- SLIGHTLY CLAYEY FINE SAND (SP-SC)
- CLAYEY FINE SAND (SC)
- SLIGHTLY SILTY FINE SAND (SP-SM)
- CEMENTED SAND AND SHELL (L)

NOTE: 3"-6" of topsoil encountered in most borings (not shown on boring profiles)

DRILLING NOTES:

TB-#	STANDARD PENETRATION TEST [SPT] BORING (ASTM D1586)	DRILL CREW CHIEF: DT
N	SPT RESISTANCE IN BLOWS PER FOOT	DRILL RIG: MOBILE B-59
	GROUNDWATER TABLE (FT-BLS) AT TIME OF DRILLING	DRILLING METHOD: ROTARY-WASH/BENTONITE SLURRY
EOB	END OF BORING	SPLIT-SPOON SAMPLER:
BLS	BELOW LAND SURFACE	INSIDE DIAMETER: 1.375"
SP, SP-SC	UNIFIED SOIL CLASSIFICATION SYSTEM [USCS]	OUTSIDE DIAMETER: 2.0"
SC, SP-SM, L	USCS GROUPS DETERMINED BY VISUAL CLASSIFICATION	LENGTH: 24"
	EXCEPT FOR NOTED LABORATORY TESTS	SPT HAMMER:
MC	NATURAL MOISTURE CONTENT IN PERCENT (ASTM D2216)	AVERAGE DROP: 30"
-200	PERCENT FINES PASSING THE NO. 200 SIEVE (ASTM D1140)	WEIGHT: 140 LBS
		TYPE: SAFETY/MANUAL



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834 SW Swan Avenue, Port St. Lucie, FL 34983 772-807-9191 www.AACEinc.com

SOIL BORING PROFILES

LIMITED SUBSURFACE SOIL EXPLORATION AND
PRELIMINARY GEOTECHNICAL ENGINEERING EVALUATION
606-ACRE PROPERTY - WARFIELD BLVD (SR-710)
PHASE 1 - PROPOSED DATA PROCESSING CENTER
INDIANTOWN, MARTIN COUNTY, FLORIDA

Drawn by: PGA

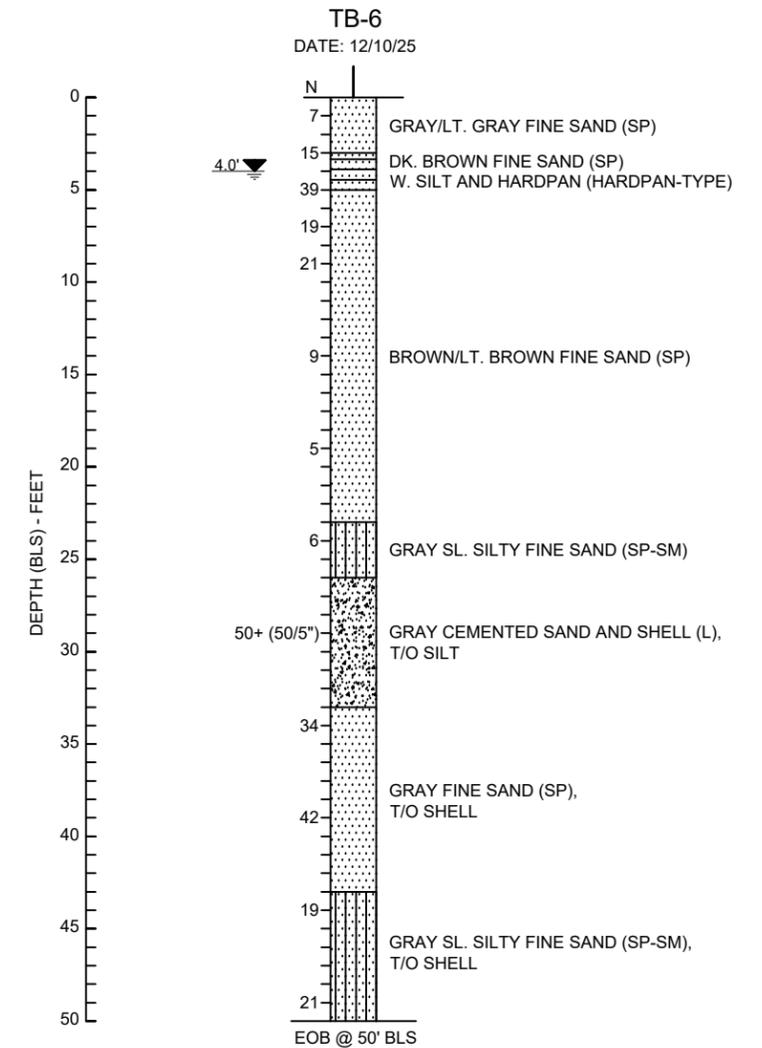
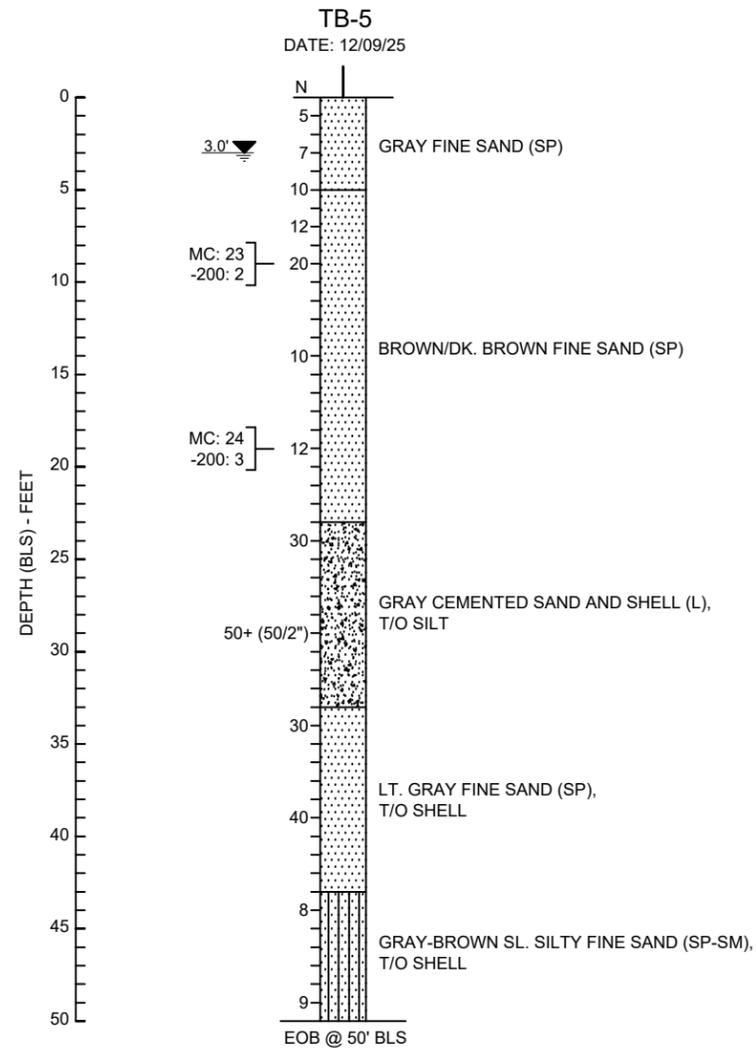
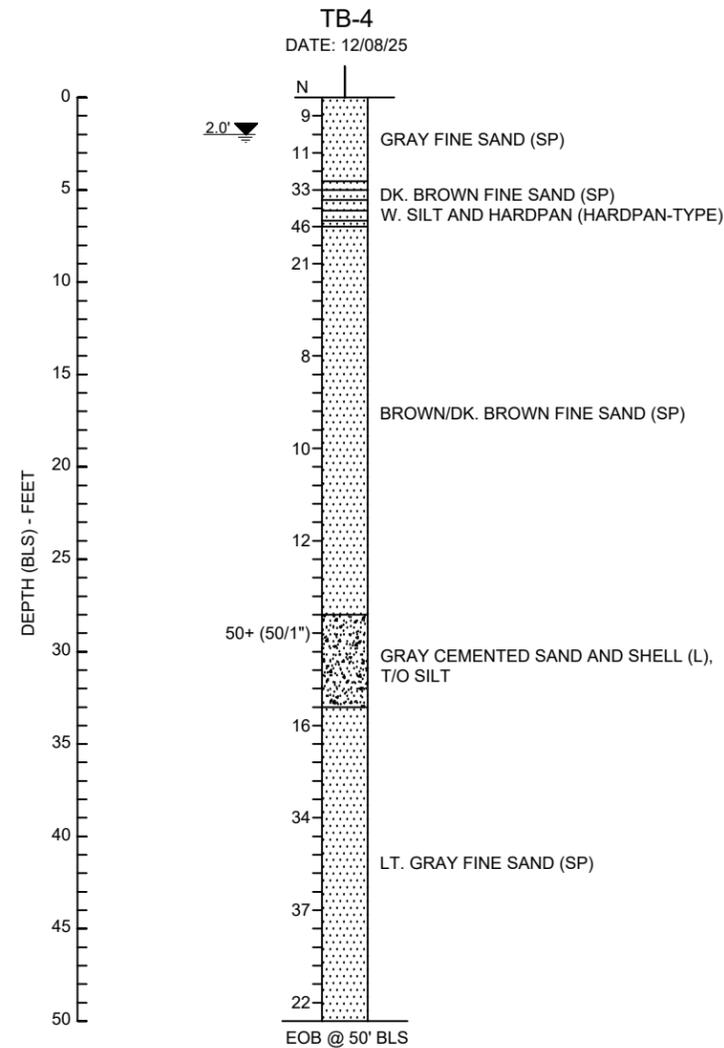
Date: December 2025

Checked by: DPA

Date: December 2025

AAACE File No: 25-235

Sheet No. 1



SOIL GRAPHICAL LEGEND:

- FINE SAND (SP)
- FINE SAND (SP) W. SILT AND HARDPAN [HARDPAN-TYPE]
- SLIGHTLY CLAYEY FINE SAND (SP-SC)
- CLAYEY FINE SAND (SC)
- SLIGHTLY SILTY FINE SAND (SP-SM)
- CEMENTED SAND AND SHELL (L)

DRILLING NOTES:

- | | | |
|--------------|--|---|
| TB-# | STANDARD PENETRATION TEST [SPT] BORING (ASTM D1586) | DRILL CREW CHIEF: DT |
| N | SPT RESISTANCE IN BLOWS PER FOOT | DRILL RIG: MOBILE B-59 |
| X-X | GROUNDWATER TABLE (FT-BLS) AT TIME OF DRILLING | DRILLING METHOD: ROTARY-WASH/BENTONITE SLURRY |
| EOB | END OF BORING | SPLIT-SPOON SAMPLER: |
| BLS | BELOW LAND SURFACE | INSIDE DIAMETER: 1.375" |
| SP, SP-SC | UNIFIED SOIL CLASSIFICATION SYSTEM [USCS] | OUTSIDE DIAMETER: 2.0" |
| SC, SP-SM, L | USCS GROUPS DETERMINED BY VISUAL CLASSIFICATION | LENGTH: 24" |
| | EXCEPT FOR NOTED LABORATORY TESTS | SPT HAMMER: |
| MC | NATURAL MOISTURE CONTENT IN PERCENT (ASTM D2216) | AVERAGE DROP: 30" |
| -200 | PERCENT FINES PASSING THE NO. 200 SIEVE (ASTM D1140) | WEIGHT: 140 LBS |
| | | TYPE: SAFETY/MANUAL |



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606-ACRE PROPERTY - WARFIELD BLVD (SR-710)
PHASE 1 - PROPOSED DATA PROCESSING CENTER
INDIANTOWN, MARTIN COUNTY, FLORIDA

Drawn by: PGA

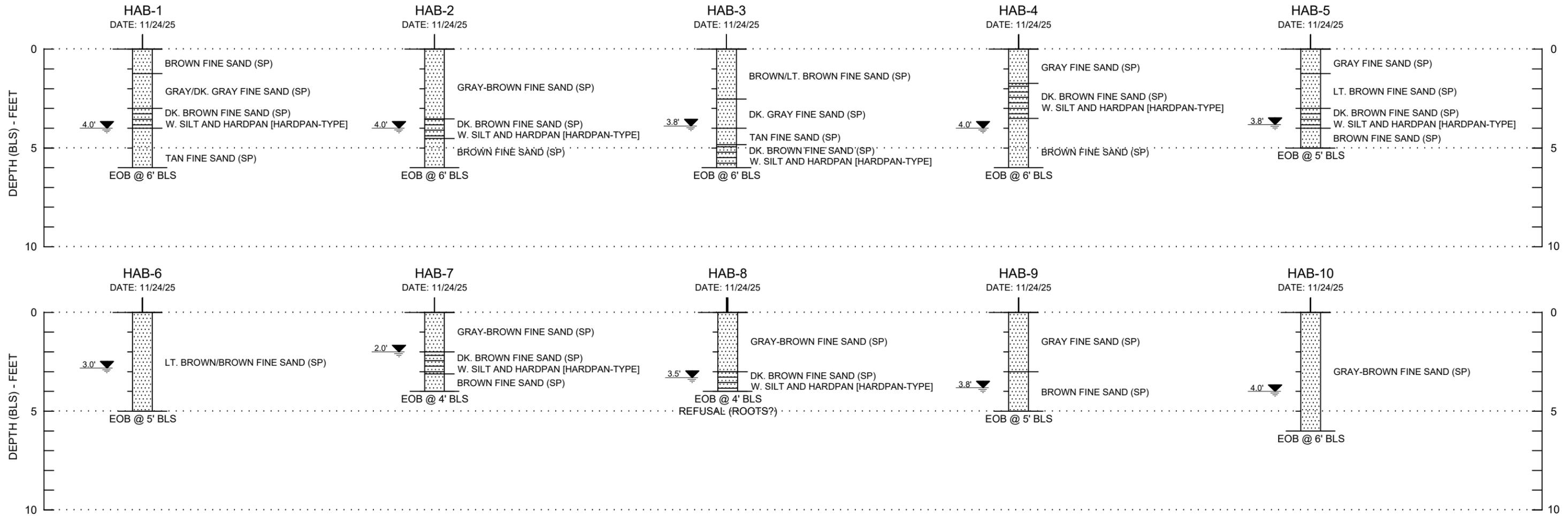
Date: December 2025

Checked by: DPA

Date: December 2025

AACE File No: 25-235

Sheet No. 2



SOIL GRAPHICAL LEGEND:

- FINE SAND (SP)
- FINE SAND (SP) W. SILT AND HARDPAN [HARDPAN-TYPE]
- SLIGHTLY CLAYEY FINE SAND (SP-SC)
- CLAYEY FINE SAND (SC)
- SLIGHTLY SILTY FINE SAND (SP-SM)
- CEMENTED SAND AND SHELL (L)

DRILLING NOTES:

- | | | |
|--------------|--|---|
| TB-# | STANDARD PENETRATION TEST [SPT] BORING (ASTM D1586) | DRILL CREW CHIEF: DT |
| N | SPT RESISTANCE IN BLOWS PER FOOT | DRILL RIG: MOBILE B-59 |
| | GROUNDWATER TABLE (FT-BLS) AT TIME OF DRILLING | DRILLING METHOD: ROTARY-WASH/BENTONITE SLURRY |
| EOB | END OF BORING | SPLIT-SPOON SAMPLER: |
| BLS | BELOW LAND SURFACE | INSIDE DIAMETER: 1.375" |
| SP, SP-SC | UNIFIED SOIL CLASSIFICATION SYSTEM [USCS] | OUTSIDE DIAMETER: 2.0" |
| SC, SP-SM, L | USCS GROUPS DETERMINED BY VISUAL CLASSIFICATION | LENGTH: 24" |
| | EXCEPT FOR NOTED LABORATORY TESTS | SPT HAMMER: |
| MC | NATURAL MOISTURE CONTENT IN PERCENT (ASTM D2216) | AVERAGE DROP: 30" |
| -200 | PERCENT FINES PASSING THE NO. 200 SIEVE (ASTM D1140) | WEIGHT: 140 LBS |
| | | TYPE: SAFETY/MANUAL |



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606-ACRE PROPERTY - WARFIELD BLVD (SR-710)
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INDIANTOWN, MARTIN COUNTY, FLORIDA

Drawn by: PGA

Checked by: DPA

AAACE File No: 25-235

Date: December 2025

Date: December 2025

Sheet No. 3

APPENDIX I

USDA NRCS Web Soil Survey Summary Report



United States
Department of
Agriculture

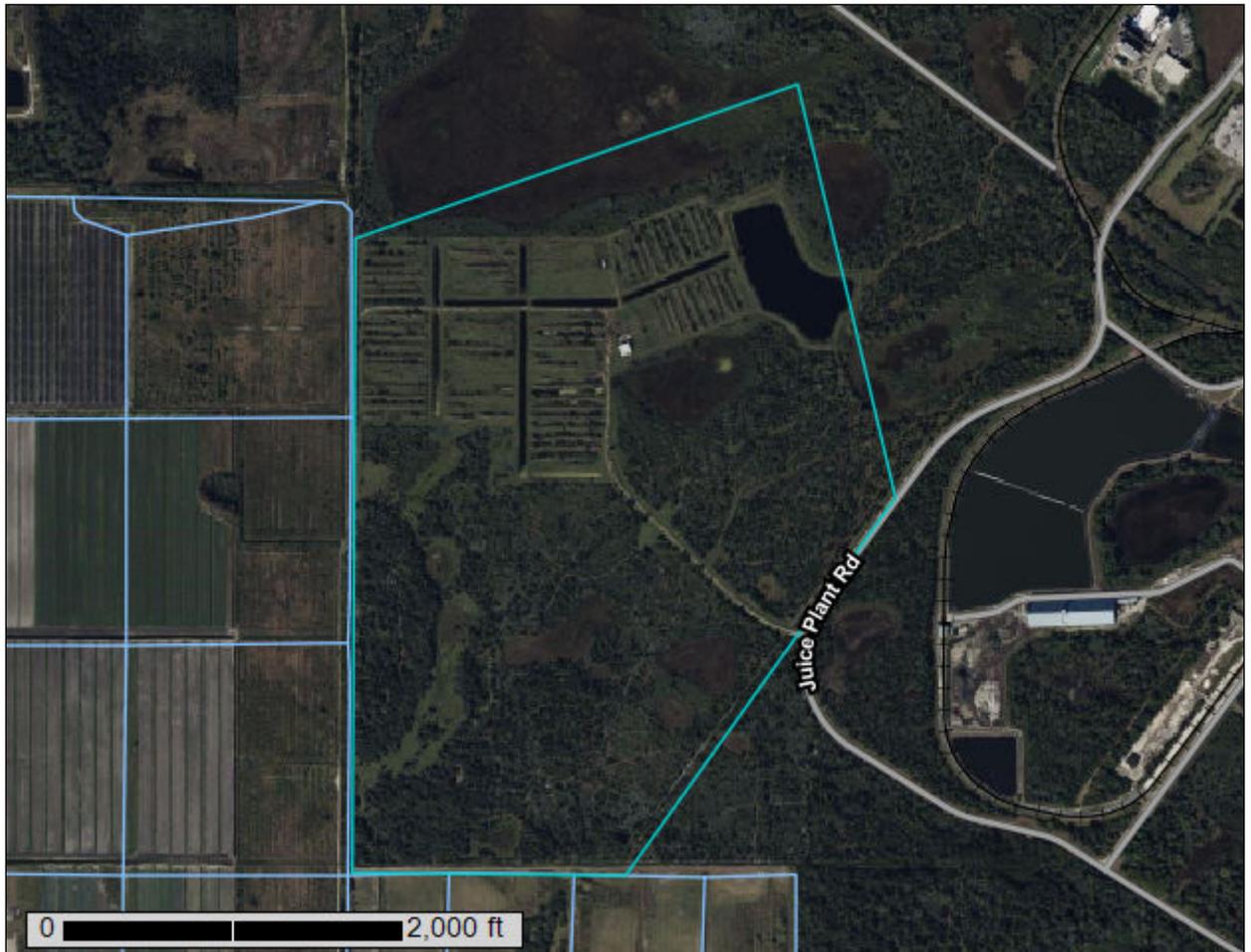
NRCS

Natural
Resources
Conservation
Service

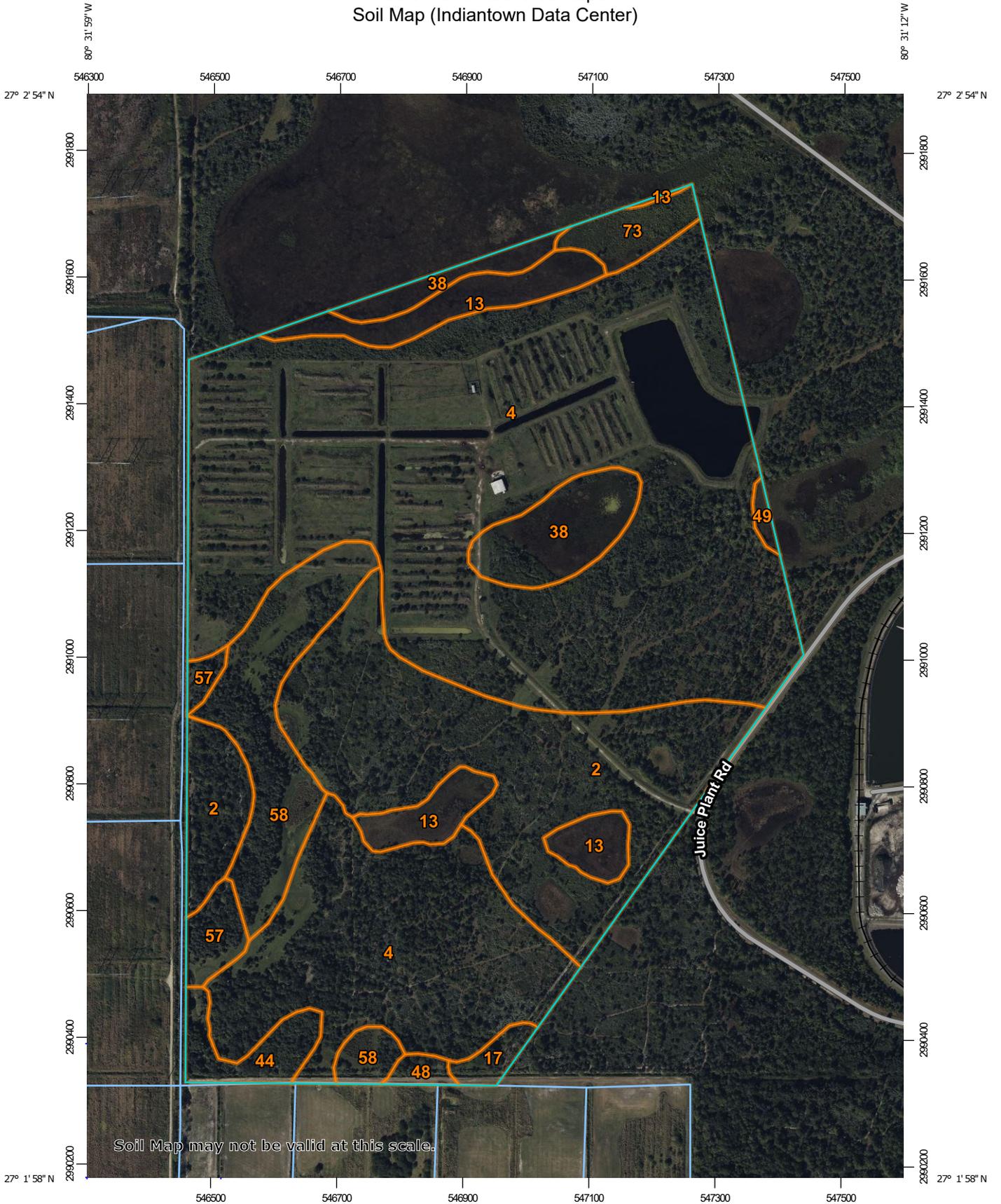
A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Martin County, Florida

Indiantown Data Center



Custom Soil Resource Report Soil Map (Indiantown Data Center)



Soil Map may not be valid at this scale.

Map Scale: 1:8,360 if printed on A portrait (8.5" x 11") sheet.

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 17N WGS84

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features

-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Martin County, Florida
 Survey Area Data: Version 24, Aug 29, 2025

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jan 18, 2022—Jan 30, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend (Indiantown Data Center)

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
2	Lawnwood and Myakka fine sands	49.4	19.0%
4	Waveland and Immokalee fine sands	154.5	59.4%
13	Placid and Basinger fine sands, depressional	12.4	4.8%
17	Wabasso sand, 0 to 2 percent slopes	1.7	0.6%
38	Floridana fine sand, frequently ponded, 0 to 1 percent slopes	10.7	4.1%
44	Cypress Lake fine sand, 0 to 2 percent slopes	4.3	1.6%
48	Jupiter sand	1.1	0.4%
49	Riviera fine sand, frequently ponded, 0 to 1 percent slopes	0.6	0.2%
57	Chobee muck, frequently ponded, 0 to 1 percent slopes	3.7	1.4%
58	Gator and Tequesta mucks	17.8	6.9%
73	Samsula muck, frequently ponded, 0 to 1 percent slopes	3.8	1.5%
Totals for Area of Interest		259.9	100.0%

Map Unit Descriptions (Indiantown Data Center)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called

Custom Soil Resource Report

noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can

Custom Soil Resource Report

be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Martin County, Florida

2—Lawnwood and Myakka fine sands

Map Unit Setting

National map unit symbol: 1jq7l
Elevation: 0 to 110 feet
Mean annual precipitation: 56 to 64 inches
Mean annual air temperature: 72 to 79 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Lawnwood and similar soils: 41 percent
Myakka and similar soils: 39 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lawnwood

Setting

Landform: Marine terraces on flatwoods
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand
E - 5 to 28 inches: fine sand
Bh - 28 to 52 inches: loamy fine sand
C1 - 52 to 64 inches: fine sand
C2 - 64 to 80 inches: loamy fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 20 to 30 inches to ortstein
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very low (about 0.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: A/D
Ecological site: F156BY040FL - Sandy Pine Flatwoods and Hammocks
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)

Custom Soil Resource Report

Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Description of Myakka

Setting

Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Sandy marine deposits

Typical profile

A - 0 to 6 inches: fine sand
E - 6 to 20 inches: fine sand
Bh - 20 to 36 inches: fine sand
C - 36 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Low (about 5.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: B/D
Ecological site: F156BY040FL - Sandy Pine Flatwoods and Hammocks
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Minor Components

Basinger

Percent of map unit: 7 percent
Landform: Drainageways on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Linear
Across-slope shape: Concave
Ecological site: R156BY021FL - Mineral Isolated Marshes and Swamps
Other vegetative classification: Slough (R156BY011FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: Yes

Placid

Percent of map unit: 7 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Ecological site: R156BY021FL - Mineral Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL),
Sandy soils on stream terraces, flood plains, or in depressions
(G156BC145FL)
Hydric soil rating: Yes

Waveland

Percent of map unit: 6 percent
Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: F156BY040FL - Sandy Pine Flatwoods and Hammocks
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy
soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

4—Waveland and Immokalee fine sands

Map Unit Setting

National map unit symbol: 1jq7n
Elevation: 0 to 80 feet
Mean annual precipitation: 56 to 64 inches
Mean annual air temperature: 72 to 79 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Waveland and similar soils: 41 percent
Immokalee and similar soils: 39 percent
Minor components: 20 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Waveland

Setting

Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Sandy marine deposits

Custom Soil Resource Report

Typical profile

A - 0 to 4 inches: fine sand
Eg - 4 to 43 inches: fine sand
Bh1 - 43 to 47 inches: fine sand
Bh2 - 47 to 77 inches: loamy fine sand
Cg1 - 77 to 91 inches: fine sand
Cg2 - 91 to 99 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 30 to 50 inches to ortstein
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very low (about 1.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: A/D
Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Description of Immokalee

Setting

Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Convex
Across-slope shape: Linear
Parent material: Sandy marine deposits

Typical profile

A - 0 to 6 inches: fine sand
E - 6 to 35 inches: fine sand
Bh - 35 to 54 inches: fine sand
BC - 54 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 6 to 18 inches

Custom Soil Resource Report

Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: B/D
Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Minor Components

Lawnwood

Percent of map unit: 4 percent
Landform: Marine terraces on flatwoods
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Basinger

Percent of map unit: 4 percent
Landform: Drainageways on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Linear
Across-slope shape: Concave
Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks
Other vegetative classification: Slough (R156BY011FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: Yes

Placid

Percent of map unit: 3 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G156BC145FL)
Hydric soil rating: Yes

Jonathan

Percent of map unit: 3 percent
Landform: Rises on marine terraces
Landform position (three-dimensional): Interfluv

Custom Soil Resource Report

Down-slope shape: Convex

Across-slope shape: Linear

Ecological site: R155XY180FL - Sandy Scrub on Rises, Ridges, and Knolls of Mesic Uplands

Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G156BC121FL)

Hydric soil rating: No

Nettles

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)

Hydric soil rating: No

Salerno

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)

Hydric soil rating: No

13—Placid and Basinger fine sands, depressional

Map Unit Setting

National map unit symbol: 1jq7x

Elevation: 0 to 50 feet

Mean annual precipitation: 56 to 64 inches

Mean annual air temperature: 72 to 79 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Farmland of unique importance

Map Unit Composition

Placid and similar soils: 45 percent

Basinger and similar soils: 40 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Placid

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Sandy marine deposits

Typical profile

A - 0 to 17 inches: fine sand
Cg - 17 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G156BC145FL)
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G156BC145FL)
Hydric soil rating: Yes

Description of Basinger

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand
Eg - 4 to 22 inches: fine sand
Bh/Eg - 22 to 42 inches: fine sand
Cg - 42 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Custom Soil Resource Report

Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Low (about 5.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G156BC145FL)
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G156BC145FL)
Hydric soil rating: Yes

Minor Components

Lawnwood

Percent of map unit: 8 percent
Landform: Marine terraces on flatwoods
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Ecological site: F156BY040FL - Sandy Pine Flatwoods and Hammocks
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Sanibel

Percent of map unit: 7 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Organic soils in depressions and on flood plains (G156BC645FL)
Hydric soil rating: Yes

17—Wabasso sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2svyr

Elevation: 0 to 70 feet

Mean annual precipitation: 46 to 55 inches

Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 355 to 365 days

Farmland classification: Farmland of unique importance

Map Unit Composition

Wabasso and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wabasso

Setting

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 6 inches: sand

E - 6 to 25 inches: sand

Bh - 25 to 30 inches: sand

Btg - 30 to 58 inches: sandy clay loam

Cg - 58 to 80 inches: loamy sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 9 to 50 inches to strongly contrasting textural stratification

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 6 to 18 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 5 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Very low (about 1.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Custom Soil Resource Report

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: C/D

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

Minor Components

Brynwood

Percent of map unit: 6 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Cypress lake

Percent of map unit: 5 percent

Landform: Drainageways on marine terraces, flats on marine terraces

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Linear, convex

Across-slope shape: Concave, linear

Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

Pineda

Percent of map unit: 4 percent

Landform: Flats on marine terraces, drainageways on marine terraces

Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Linear

Across-slope shape: Linear, concave

Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks

Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

38—Floridana fine sand, frequently ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2sm53

Elevation: 0 to 90 feet

Mean annual precipitation: 42 to 64 inches

Custom Soil Resource Report

Mean annual air temperature: 70 to 77 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Floridana and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Floridana

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Linear, concave
Across-slope shape: Linear, concave
Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 19 inches: fine sand
Eg - 19 to 25 inches: fine sand
Btg - 25 to 80 inches: fine sandy loam

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 10 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: C/D
Ecological site: R155XY080FL - Sandy over Loamy Freshwater Isolated Marshes and Swamps
Forage suitability group: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)
Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)
Hydric soil rating: Yes

Minor Components

Tequesta

Percent of map unit: 4 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip

Custom Soil Resource Report

Down-slope shape: Concave
Across-slope shape: Concave
Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Organic soils in depressions and on flood plains (G156AC645FL)
Hydric soil rating: Yes

Gator

Percent of map unit: 3 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Concave
Across-slope shape: Concave
Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Organic soils in depressions and on flood plains (G155XB645FL)
Hydric soil rating: Yes

Anclote

Percent of map unit: 3 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Convex, concave
Across-slope shape: Linear, concave
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL)
Hydric soil rating: Yes

Riviera

Percent of map unit: 3 percent
Landform: Flatwoods on marine terraces, drainageways on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Linear
Across-slope shape: Linear, concave
Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

Felda

Percent of map unit: 2 percent
Landform: Flatwoods on marine terraces, drainageways on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Linear
Across-slope shape: Linear, concave
Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

44—Cypress Lake fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2zldq
Elevation: 0 to 40 feet
Mean annual precipitation: 55 to 63 inches
Mean annual air temperature: 68 to 77 degrees F
Frost-free period: 355 to 365 days
Farmland classification: Not prime farmland

Map Unit Composition

Cypress lake, nonhydic, and similar soils: 70 percent
Cypress lake, hydric, and similar soils: 15 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Cypress Lake, Nonhydic

Setting

Landform: Flats on marine terraces
Landform position (three-dimensional): Tread, talf
Down-slope shape: Convex
Across-slope shape: Linear
Parent material: Sandy and loamy marine deposits over limestone over sandy marine deposits

Typical profile

A - 0 to 7 inches: fine sand
E - 7 to 25 inches: fine sand
Btg - 25 to 32 inches: fine sandy loam
2R - 32 to 40 inches: bedrock
3C1 - 40 to 50 inches: fine sand
3C2 - 50 to 81 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 9 to 58 inches to lithic bedrock
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very low (about 2.9 inches)

Custom Soil Resource Report

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: A/D
Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks
Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G156BC241FL)
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G156BC241FL)
Hydric soil rating: No

Description of Cypress Lake, Hydric

Setting

Landform: Flats on marine terraces
Landform position (three-dimensional): Tread, talf
Down-slope shape: Linear
Across-slope shape: Linear, concave
Parent material: Sandy and loamy marine deposits over limestone over sandy marine deposits

Typical profile

A - 0 to 7 inches: fine sand
E - 7 to 25 inches: fine sand
Btg - 25 to 32 inches: fine sandy loam
2R - 32 to 40 inches: bedrock
3C1 - 40 to 50 inches: fine sand
3C2 - 50 to 81 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 9 to 58 inches to lithic bedrock
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very low (about 2.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: A/D
Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks
Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G156BC241FL)
Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G156BC241FL)
Hydric soil rating: Yes

Minor Components

Riviera

Percent of map unit: 3 percent

Landform: Flats on marine terraces, drainageways on marine terraces

Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Linear

Across-slope shape: Linear, concave

Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks

Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

Wabasso

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear, convex

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

Brynwood

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Pineda

Percent of map unit: 3 percent

Landform: Flats on marine terraces, drainageways on marine terraces

Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Linear

Across-slope shape: Linear, concave

Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks

Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

Pinellas

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks

Other vegetative classification: Cabbage Palm Flatwoods (R155XY005FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: No

48—Jupiter sand

Map Unit Setting

National map unit symbol: 1jq8v

Elevation: 10 to 30 feet

Mean annual precipitation: 56 to 64 inches

Mean annual air temperature: 72 to 79 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Farmland of unique importance

Map Unit Composition

Jupiter, nonhydic, and similar soils: 60 percent

Jupiter, hydric, and similar soils: 20 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Jupiter, Nonhydic

Setting

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Convex

Across-slope shape: Linear

Parent material: Sandy marine deposits over limestone

Typical profile

Ap1 - 0 to 4 inches: sand

A2 - 4 to 10 inches: sand

2R - 10 to 22 inches: unweathered bedrock

3C1 - 22 to 32 inches: sandy clay loam

3C2 - 32 to 48 inches: sandy loam

3C3 - 48 to 72 inches: fine sandy loam

3C4 - 72 to 80 inches: loamy sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: 8 to 20 inches to lithic bedrock

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 6 to 18 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum content: 30 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Very low (about 0.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: D
Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Other vegetative classification: Wetland Hardwood Hammock (R156BY012FL),
Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: No

Description of Jupiter, Hydric

Setting

Landform: Drainageways on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Linear
Across-slope shape: Concave
Parent material: Sandy marine deposits over limestone

Typical profile

Ap1 - 0 to 4 inches: mucky fine sand
A2 - 4 to 10 inches: sand
2R - 10 to 22 inches: unweathered bedrock
3C1 - 22 to 32 inches: sandy clay loam
3C2 - 32 to 48 inches: sandy loam
3C3 - 48 to 72 inches: fine sandy loam
3C4 - 72 to 80 inches: loamy sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: 8 to 20 inches to lithic bedrock
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 30 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: Very low (about 0.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 4w
Hydrologic Soil Group: D
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Other vegetative classification: Wetland Hardwood Hammock (R156BY012FL),
Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)
Hydric soil rating: Yes

Minor Components

Canova variant, drained

Percent of map unit: 4 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps

Other vegetative classification: Organic soils in depressions and on flood plains (G156BC645FL)

Hydric soil rating: Yes

Hallandale, hydric

Percent of map unit: 4 percent

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Ecological site: R156AY320FL - Subtropical Freshwater Non-Forested Wetlands of Miami Ridge/ Atlantic Coastal Strip

Other vegetative classification: South Florida Flatwoods (R156BY003FL), Sandy soils on flats of mesic or hydric lowlands (G156BC141FL)

Hydric soil rating: Yes

Chobee

Percent of map unit: 4 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY090FL - Loamy and Clayey Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Loamy and clayey soils on stream terraces, flood plains, or in depressions (G156BC345FL)

Hydric soil rating: Yes

Floridana

Percent of map unit: 4 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY080FL - Sandy over Loamy Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G156BC245FL)

Hydric soil rating: Yes

Pinellas

Percent of map unit: 4 percent

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Custom Soil Resource Report

Down-slope shape: Convex
Across-slope shape: Linear
Ecological site: F155XY130FL - Sandy over Loamy Flatwoods and Hammocks
Other vegetative classification: Wetland Hardwood Hammock (R156BY012FL),
Sandy over loamy soils on flats of hydric or mesic lowlands (G156BC241FL)
Hydric soil rating: No

49—Riviera fine sand, frequently ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2tzwl
Elevation: 0 to 80 feet
Mean annual precipitation: 44 to 64 inches
Mean annual air temperature: 68 to 77 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Riviera and similar soils: 85 percent
Minor components: 15 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Riviera

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 4 inches: fine sand
E - 4 to 36 inches: fine sand
Bt/E - 36 to 42 inches: fine sandy loam
Cg1 - 42 to 56 inches: fine sand
Cg2 - 56 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high
(0.60 to 2.00 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Custom Soil Resource Report

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Low (about 5.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: A/D

Ecological site: R155XY080FL - Sandy over Loamy Freshwater Isolated Marshes and Swamps

Forage suitability group: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)

Hydric soil rating: Yes

Minor Components

Chobee

Percent of map unit: 7 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY090FL - Loamy and Clayey Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Loamy and clayey soils on stream terraces, flood plains, or in depressions (G156BC345FL)

Hydric soil rating: Yes

Tequesta

Percent of map unit: 4 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Organic soils in depressions and on flood plains (G156AC645FL)

Hydric soil rating: Yes

Wabasso

Percent of map unit: 4 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear, convex

Across-slope shape: Linear

Ecological site: F155XY120FL - Sandy Flatwoods and Hammocks

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

57—Chobee muck, frequently ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2tzwg
Elevation: 0 to 130 feet
Mean annual precipitation: 43 to 64 inches
Mean annual air temperature: 70 to 77 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Chobee and similar soils: 90 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Chobee

Setting

Landform: Depressions on flatwoods on marine terraces
Landform position (three-dimensional): Tread, dip, talf
Down-slope shape: Linear, concave
Across-slope shape: Linear, concave
Parent material: Loamy alluvium

Typical profile

Oa - 0 to 4 inches: muck
A - 4 to 16 inches: loamy sand
Btg1 - 16 to 28 inches: fine sandy loam
Btg2 - 28 to 42 inches: sandy clay loam
Btg3 - 42 to 53 inches: fine sandy loam
Cg - 53 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 7 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 2.0
Available water supply, 0 to 60 inches: Moderate (about 8.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w

Custom Soil Resource Report

Hydrologic Soil Group: C/D

Ecological site: R156BY021FL - Mineral Isolated Marshes and Swamps

Forage suitability group: Organic soils in depressions and on flood plains
(G155XB645FL)

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL),
Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Minor Components

Riviera

Percent of map unit: 4 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R156BY021FL - Mineral Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL),
Sandy over loamy soils on stream terraces, flood plains, or in depressions
(G155XB245FL)

Hydric soil rating: Yes

Gator

Percent of map unit: 3 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R156BY020FL - Histisol Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL),
Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Tequesta

Percent of map unit: 3 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R156BY021FL - Mineral Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL),
Organic soils in depressions and on flood plains (G156AC645FL)

Hydric soil rating: Yes

58—Gator and Tequesta mucks

Map Unit Setting

National map unit symbol: 1jq98

Elevation: 0 to 60 feet

Mean annual precipitation: 56 to 64 inches

Custom Soil Resource Report

Mean annual air temperature: 72 to 79 degrees F
Frost-free period: 350 to 365 days
Farmland classification: Farmland of unique importance

Map Unit Composition

Gator and similar soils: 50 percent
Tequesta and similar soils: 40 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Gator

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave
Across-slope shape: Concave
Parent material: Herbaceous organic material over loamy and sandy marine deposits

Typical profile

Oa - 0 to 24 inches: muck
Cg1 - 24 to 48 inches: fine sandy loam
Cg2 - 48 to 56 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 1.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water supply, 0 to 60 inches: High (about 11.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: B/D
Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps
Forage suitability group: Organic soils in depressions and on flood plains (G156BC645FL)
Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Organic soils in depressions and on flood plains (G156BC645FL)
Hydric soil rating: Yes

Description of Tequesta

Setting

Landform: Depressions on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Concave

Custom Soil Resource Report

Across-slope shape: Concave

Parent material: Stratified sandy and loamy marine deposits

Typical profile

Oa - 0 to 14 inches: muck

A - 14 to 26 inches: sand

Eg - 26 to 30 inches: sand

Btg - 30 to 40 inches: sandy clay loam

B/C - 40 to 48 inches: loamy sand

Cg - 48 to 64 inches: sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.60 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None

Frequency of ponding: Frequent

Calcium carbonate, maximum content: 5 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: C/D

Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps

Forage suitability group: Organic soils in depressions and on flood plains (G156BC645FL)

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Organic soils in depressions and on flood plains (G156BC645FL)

Hydric soil rating: Yes

Minor Components

Floridana

Percent of map unit: 5 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY080FL - Sandy over Loamy Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G156BC245FL)

Hydric soil rating: Yes

Chobee

Percent of map unit: 5 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Dip

Custom Soil Resource Report

Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: R155XY090FL - Loamy and Clayey Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL),
Loamy and clayey soils on stream terraces, flood plains, or in depressions
(G156BC345FL)

Hydric soil rating: Yes

73—Samsula muck, frequently ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2tzw9

Elevation: 0 to 250 feet

Mean annual precipitation: 44 to 63 inches

Mean annual air temperature: 68 to 77 degrees F

Frost-free period: 335 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Samsula and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Samsula

Setting

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave

Across-slope shape: Concave

Parent material: Herbaceous organic material over sandy marine deposits

Typical profile

Oa1 - 0 to 24 inches: muck

Oa2 - 24 to 32 inches: muck

Cg1 - 32 to 35 inches: sand

Cg2 - 35 to 44 inches: sand

Cg3 - 44 to 80 inches: sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None

Custom Soil Resource Report

Frequency of ponding: Frequent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Sodium adsorption ratio, maximum: 4.0

Available water supply, 0 to 60 inches: Very high (about 13.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: A/D

Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps

Forage suitability group: Organic soils in depressions and on flood plains (G155XB645FL)

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Minor Components

Basinger

Percent of map unit: 3 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave, linear

Across-slope shape: Concave, linear

Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Kaliga

Percent of map unit: 3 percent

Landform: Depressions on flatwoods on marine terraces

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Linear, concave

Across-slope shape: Linear, concave

Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Myakka

Percent of map unit: 3 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip

Down-slope shape: Linear, concave

Across-slope shape: Linear, concave

Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL)

Hydric soil rating: Yes

Sanibel

Percent of map unit: 2 percent

Landform: Depressions on marine terraces

Custom Soil Resource Report

Landform position (three-dimensional): Tread, dip
Down-slope shape: Linear, concave
Across-slope shape: Concave
Ecological site: R155XY100FL - Organic Freshwater Isolated Marshes and Swamps
Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL)
Hydric soil rating: Yes

Anclote

Percent of map unit: 2 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Convex, concave
Across-slope shape: Linear, concave
Ecological site: R155XY070FL - Sandy Freshwater Isolated Marshes and Swamps
Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL)
Hydric soil rating: Yes

Floridana

Percent of map unit: 2 percent
Landform: Depressions on marine terraces
Landform position (three-dimensional): Tread, dip
Down-slope shape: Concave, linear
Across-slope shape: Concave, linear
Ecological site: R155XY080FL - Sandy over Loamy Freshwater Isolated Marshes and Swamps
Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)
Hydric soil rating: Yes

APPENDIX II

General Notes

ANDERSEN ANDRE CONSULTING ENGINEERS, INC.
SOIL BORING, SAMPLING AND TESTING METHODS

GENERAL

Andersen Andre Consulting Engineers, Inc. (AACE) borings describe subsurface conditions only at the locations drilled and at the time drilled. They provide no information about subsurface conditions below the bottom of the boreholes. At locations not explored, surface conditions that differ from those observed in the borings may exist and should be anticipated.

The information reported on our boring logs is based on our drillers' logs and on visual examination in our laboratory of disturbed soil samples recovered from the borings. The distinction shown on the logs between soil types is approximate only. The actual transition from one soil to another may be gradual and indistinct.

The groundwater depth shown on our boring logs is the water level the driller observed in the borehole when it was drilled. These water levels may have been influenced by the drilling procedures, especially in borings made by rotary drilling with bentonitic drilling mud. An accurate determination of groundwater level requires long-term observation of suitable monitoring wells. Fluctuations in groundwater levels throughout the year should be anticipated.

The absence of a groundwater level on certain logs indicates that no groundwater data is available. It does not mean that groundwater will not be encountered at that boring location at some other point in time.

STANDARD PENETRATION TEST

The Standard Penetration Test (SPT) is a widely accepted method of in situ testing of foundation soils (ASTM D-1586). A 2-foot (0.6m) long, 2-inch (50mm) O.D. split-barrell sampler attached to the end of a string of drilling rods is driven 24 inches (0.60m) into the ground by successive blows of a 140-pound (63.5 Kg) hammer freely dropping 30 inches (0.76m). The number of blows needed for each 6 inches (0.15m) increments penetration is recorded. The sum of the blows required for penetration of the middle two 6-inch (0.15m) increments of penetration constitutes the test result of N-value. After the test, the sampler is extracted from the ground and opened to allow visual description of the retained soil sample. The N-value has been empirically correlated with various soil properties allowing a conservative estimate of the behavior of soils under load. The following tables relate N-values to a qualitative description of soil density and, for cohesive soils, an approximate unconfined compressive strength (Qu):

Cohesionless Soils:	<u>N-Value</u>	<u>Description</u>
	0 to 4	Very loose
	4 to 10	Loose
	10 to 30	Medium dense
	30 to 50	Dense
	Above 50	Very dense

Cohesive Soils:	<u>N-Value</u>	<u>Description</u>	<u>Qu</u>
	0 to 2	Very soft	Below 0.25 tsf (25 kPa)
	2 to 4	Soft	0.25 to 0.50 tsf (25 to 50 kPa)
	4 to 8	Medium stiff	0.50 to 1.0 tsf (50 to 100 kPa)
	8 to 15	Stiff	1.0 to 2.0 tsf (100 to 200 kPa)
	15 to 30	Very stiff	2.0 to 4.0 tsf (200 to 400 kPa)
	Above 30	Hard	Above 4.0 tsf (400 kPa)

The tests are usually performed at 5 foot (1.5m) intervals. However, more frequent or continuous testing is done by AACE through depths where a more accurate definition of the soils is required. The test holes are advanced to the test elevations by rotary drilling with a cutting bit, using circulating fluid to remove the cuttings and hold the fine grains in suspension. The circulating fluid, which is bentonitic drilling mud, is also used to keep the hole open below the water table by maintaining an excess hydrostatic pressure inside the hole. In some soil deposits, particularly highly pervious ones, flush-coupled casing must be driven to just above the testing depth to keep the hole open and/or prevent the loss of circulating fluid. After completion of a test borings, the hole is kept open until a steady state groundwater level is recorded. The hole is then sealed by backfilling, either with accumulated cuttings or lean cement.

Representative split-spoon samples from each sampling interval and from different strata are brought to our laboratory in air-tight jars for classification and testing, if necessary. Afterwards, the samples are discarded unless prior arrangement have been made.

POWER AUGER BORINGS

Auger borings (ASTM D-1452) are used when a relatively large, continuous sampling of soil strata close to the ground surface is desired. A 4-inch (100 mm) diameter, continuous flight, helical auger with a cutting head at its end is screwed into the ground in 5-foot (1.5m) sections. It is powered by the rotary drill rig. The sample is recovered by withdrawing the auger out of the ground without rotating it. The soil sample so obtained, is classified in the field and representative samples placed in bags or jars and returned to the AACE soils laboratory for classification and testing, if necessary.

HAND AUGER BORINGS

Hand auger borings are used, if soil conditions are favorable, when the soil strata are to be determined within a shallow (approximately 5-foot [1.5m]) depth or when access is not available to power drilling equipment. A 3-inch (75mm) diameter hand bucket auger with a cutting head is simultaneously turned and pressed into the ground. The bucket auger is retrieved at approximately 6-inch (0.15m) interval and its contents emptied for inspection. On occasion post-hole diggers are used, especially in the upper 3 feet (1m) or so. Penetrometer probings can be used in the upper 5 feet (1.5m) to determine the relative density of the soils. The soil sample obtained is described and representative samples put in bags or jars and transported to the AACE soils laboratory for classification and testing, if necessary.

UNDISTURBED SAMPLING

Undisturbed sampling (ASTM D-1587) implies the recovery of soil samples in a state as close to their natural condition as possible. Complete preservation of in situ conditions cannot be realized; however, with careful handling and proper sampling techniques, disturbance during sampling can be minimized for most geotechnical engineering purposes. Testing of undisturbed samples gives a more accurate estimate of in situ behavior than is possible with disturbed samples.

Normally, we obtain undisturbed samples by pushing a 2.875-inch (73 mm) I.D., thin wall seamless steel tube 24 inches (0.6 m) into the soil with a single stoke of a hydraulic ram. The sampler, which is a Shelby tube, is 30 (0.8 m) inches long. After the sampler is retrieved, the ends are sealed in the field and it is transported to our laboratory for visual description and testing, as needed.

ROCK CORING

In case rock strata is encountered and rock strength/continuity/composition information is needed for foundation or mining purposes, the rock can be cored (ASTM D-2113) and 2-inch to 4-inch diameter rock core samples be obtained for further laboratory analyses. The rock coring is performed through flush-joint steel casing temporarily installed through the overburden soils above the rock formation and also installed into the rock. The double- or triple-tube core barrels are advanced into the rock typically in 5-foot intervals and then retrieved to the surface. The barrel is then opened so that the core sample can be extruded. Preliminary field measurements of the recovered rock cores include percent recovery and Rock Quality Designation (RQD) values. The rock cores are placed in secure core boxes and then transported to our laboratory for further inspection and testing, as needed.

SFWMD EXFILTRATION TESTS

In order to estimate the hydraulic conductivity of the upper soils, constant head or falling head exfiltration tests can be performed. These tests are performed in accordance with methods described in the South Florida Water Management District (SFWMD) Permit Information Manual, Volume IV. In brief, a 6 to 9 inch diameter hole is augered to depths of about 5 to 7 feet; the bottom one foot is filled with 57-stone; and a 6-foot long slotted PVC pipe is lowered into the hole. The distance from the groundwater table and to the ground surface is recorded and the hole is then saturated for 10 minutes with the water level maintained at the ground surface.

If a constant head test is performed, the rate of pumping will be recorded at fixed intervals of 1 minute for a total of 10 minutes, following the saturation period.

LABORATORY TEST METHODS

Soil samples returned to the AACE soils laboratory are visually observed by a geotechnical engineer or a trained technician to obtain more accurate description of the soil strata. Laboratory testing is performed on selected samples as deemed necessary to aid in soil classification and to help define engineering properties of the soils. The test results are presented on the soil boring logs at the depths at which the respective sample was recovered, except that grain size distributions or selected other test results may be presented on separate tables, figures or plates as discussed in this report.

THE PROJECT SOIL DESCRIPTION PROCEDURE FOR SOUTHEAST FLORIDA
CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES

The soil descriptions shown on the logs are based upon visual-manual procedures in accordance with local practice. Soil classification is performed in general accordance with the United Soil Classification System and is also based on visual-manual procedures.

BOULDERS (>12" [300 MM]) and COBBLES (3" [75 MM] TO 12" [300 MM]):

GRAVEL: Coarse Gravel: 3/4" (19 mm) to 3" (75 mm)
 Fine Gravel: No. 4 (4.75 mm) Sieve to 3/4" (19 mm)

Descriptive adjectives:

0 - 5%	– no mention of gravel in description
5 - 15%	– trace
15 - 29%	– some
30 - 49%	– gravelly (shell, limerock, cemented sands)

SANDS:

COARSE SAND: No. 10 (2 mm) Sieve to No. 4 (4.75 mm) Sieve
 MEDIUM SAND: No. 40 (425 μm) Sieve to No. 10 (2 mm) Sieve
 FINE SAND: No. 200 (75 μm) Sieve to No. 40 (425 μm) Sieve

Descriptive adjectives:

0 - 5%	– no mention of sand in description
5 - 15%	– trace
15 - 29%	– some
30 - 49%	– sandy

SILT/CLAY: < #200 (75μM) Sieve

SILTY OR SILT: PI < 4
 SILTY CLAYEY OR SILTY CLAY: 4 ≤ PI ≤ 7
 CLAYEY OR CLAY: PI > 7

Descriptive adjectives:

< - 5%	– clean (no mention of silt or clay in description)
5 - 15%	– slightly
16 - 35%	– clayey, silty, or silty clayey
36 - 49%	– very

ORGANIC SOILS:

Organic Content	Descriptive Adjectives	Classification
0 - 2.5%	Usually no mention of organics in description	See Above
2.6 - 5%	slightly organic	add "with organic fines" to group name
5 - 30%	organic	SM with organic fines Organic Silt (OL) Organic Clay (OL) Organic Silt (OH)

**THE PROJECT SOIL DESCRIPTION PROCEDURE FOR SOUTHEAST FLORIDA
CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES**

Organic Clay (OH)

HIGHLY ORGANIC SOILS AND MATTER:

Organic Content	Descriptive Adjectives	Classification
30 - 75%	sandy peat	Peat (PT)
	silty peat	Peat (PT)
> 75%	amorphous peat	Peat (PT)
	fibrous peat	Peat (PT)

STRATIFICATION AND STRUCTURE:

<u>Descriptive Term</u>	<u>Thickness</u>
with interbedded	
seam	-- less than ½ inch (13 mm) thick
layer	-- ½ to 12-inches (300 mm) thick
stratum	-- more than 12-inches (300 mm) thick
pocket	-- small, erratic deposit, usually less than 1-foot
lens	-- lenticular deposits
occasional	-- one or less per foot of thickness
frequent	-- more than one per foot of thickness
calcareous	-- containing calcium carbonate (reaction to diluted HCL)
hardpan	-- spodic horizon usually medium dense
marl	-- mixture of carbonate clays, silts, shells and sands

ROCK CLASSIFICATION (FLORIDA) CHART:

<u>Symbol</u>	<u>Typical Description</u>
LS	Hard Bedded Limestone or Caprock
WLS	Fractured or Weathered Limestone
LR	Limerock (gravel, sand, silt and clay mixture)
SLS	Stratified Limestone and Soils

THE PROJECT SOIL DESCRIPTION PROCEDURE FOR SOUTHEAST FLORIDA
CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES

LEGEND FOR BORING LOGS

N:	Number of blows to drive a 2-inch OD split spoon sampler 12 inches using a 140-pound hammer dropped 30 inches
R:	Refusal (less than six inches advance of the split spoon after 50 hammer blows)
MC:	Moisture content (percent of dry weight)
OC:	Organic content (percent of dry weight)
PL:	Moisture content at the plastic limit
LL:	Moisture content at the liquid limit
PI:	Plasticity index (LL-PL)
qu:	Unconfined compressive strength (tons per square foot, unless otherwise noted)
-200:	Percent passing a No. 200 sieve (200 wash)
+40:	Percent retained above a No. 40 sieve
US:	Undisturbed sample obtained with a thin-wall Shelby tube
k:	Permeability (feet per minute, unless otherwise noted)
DD:	Dry density (pounds per cubic foot)
TW:	Total unit weight (pounds per cubic foot)

APPENDIX III

Soil Hydraulic Conductivity Test Reports

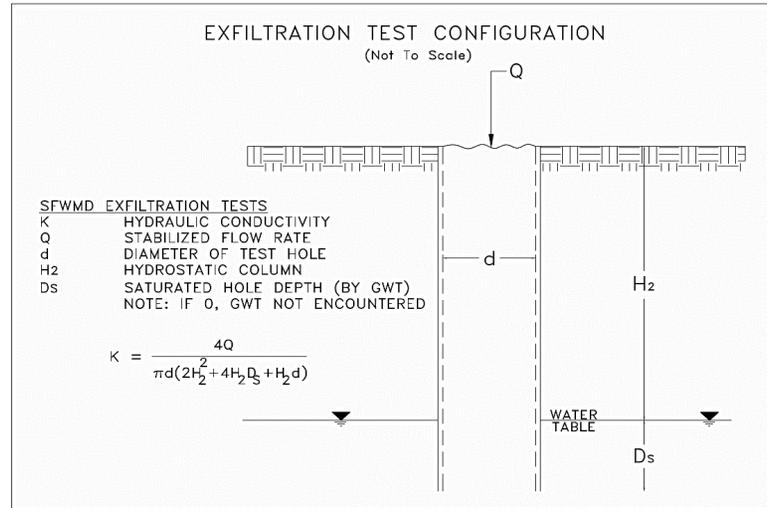


ANDERSEN ANDRE CONSULTING ENGINEERS, INC.

SFWMD Usual Open Hole Test

Test Number	EX-1	Project Name	Indiantown Data Center	Weather Conditions	Clear
		Project Number	25-235	Temperature	82F
		Test Location	Refer to Figure No. 2	Technician	DTH
		Date	12/9/2025	Engineer	PA

DIAMETER OF TEST HOLE (FEET): $d =$	0.5
DEPTH OF TEST HOLE (FEET): $H_1 =$	6
DEPTH TO WATER TABLE (FEET): $H_2 =$	2
SATURATED HOLE DEPTH (FEET): $D_s =$	4
METER READING (Gallons): $V_1 =$	0 @ 0.00 MIN
METER READING (Gallons): $V_F =$	0.9 @ 10.00 MIN
AVERAGE FLOW RATE (GPM) =	0.09
"STABILIZED" FLOW RATE (CFS): $Q =$	2.0E-04
HYDRAULIC CONDUCTIVITY (CFS / FT² - FT. HEAD): $K =$	1.2E-05



Soil Profile	
Depth (in-bls)	Description
0 - 12	Light gray fine sand (SP)
12 - 60	Dark brown fine sand (SP), traces of hardpan
60 - 72	Dark brown clayey fine sand (SC)
Groundwater encountered @ 24" below grade	

NOTES:
 The hydraulic conductivity test was performed in general accordance with the methods described in the South Florida Water Management District (SFWMD) Environmental Resource Permit Information Manual (Volume IV).
 The K-value was calculated based on the exfiltration test procedure as shown hereon.
 The presented hydraulic conductivity (K) value is applicable for an exfiltration trench installed at the same depth as the borehole test. The K-value represents an ultimate value. The designer should decide on the required factor of safety (minimum of 2, per SFWMD).

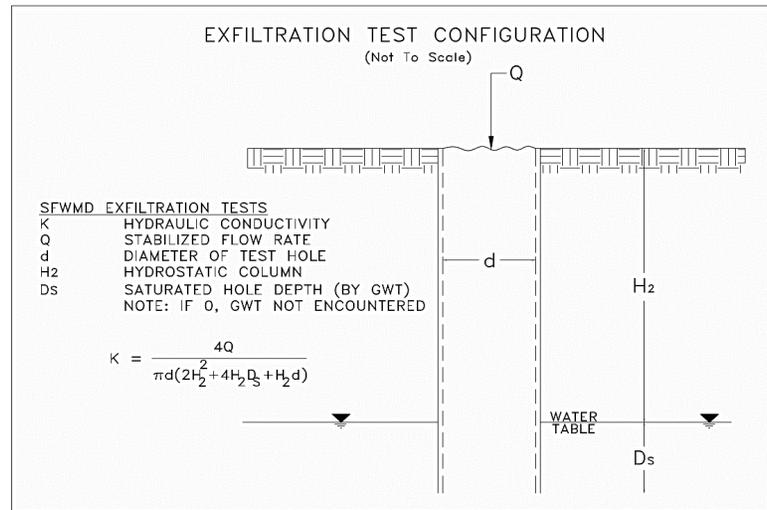


ANDERSEN ANDRE CONSULTING ENGINEERS, INC.

SFWMD Usual Open Hole Test

Test Number	EX-2	Project Name	Indiantown Data Center	Weather Conditions	Clear
		Project Number	25-235	Temperature	84F
		Test Location	Refer to Figure No. 2	Technician	DTH
		Date	12/8/2025	Engineer	PA

DIAMETER OF TEST HOLE (FEET): $d =$	0.5
DEPTH OF TEST HOLE (FEET): $H_1 =$	6
DEPTH TO WATER TABLE (FEET): $H_2 =$	3
SATURATED HOLE DEPTH (FEET): $D_s =$	3
METER READING (Gallons): $V_1 =$	0 @ 0.00 MIN
METER READING (Gallons): $V_F =$	20 @ 10.00 MIN
AVERAGE FLOW RATE (GPM) =	2.00
"STABILIZED" FLOW RATE (CFS): $Q =$	4.5E-03
HYDRAULIC CONDUCTIVITY (CFS / FT² - FT. HEAD): $K =$	2.0E-04



Soil Profile	
Depth (in-bls)	Description
0 - 72	Gray to light gray fine sand (SP)
Groundwater not encountered	

NOTES:
 The hydraulic conductivity test was performed in general accordance with the methods described in the South Florida Water Management District (SFWMD) Environmental Resource Permit Information Manual (Volume IV).
 The K-value was calculated based on the exfiltration test procedure as shown hereon.
 The presented hydraulic conductivity (K) value is applicable for an exfiltration trench installed at the same depth as the borehole test. The K-value represents an ultimate value. The designer should decide on the required factor of safety (minimum of 2, per SFWMD).

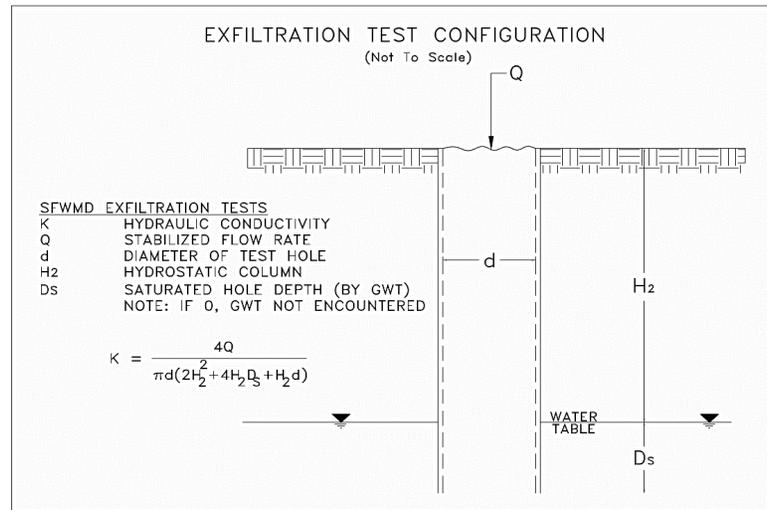


ANDERSEN ANDRE CONSULTING ENGINEERS, INC.

SFWMD Usual Open Hole Test

Test Number	EX-3	Project Name	Indiantown Data Center	Weather Conditions	Clear
		Project Number	25-235	Temperature	84F
		Test Location	Refer to Figure No. 2	Technician	DTH
		Date	12/10/2025	Engineer	PA

DIAMETER OF TEST HOLE (FEET): $d =$	0.5	
DEPTH OF TEST HOLE (FEET): $H_1 =$	6	
DEPTH TO WATER TABLE (FEET): $H_2 =$	2	
SATURATED HOLE DEPTH (FEET): $D_s =$	4	
METER READING (Gallons): $V_1 =$	0	@ 0.00 MIN
METER READING (Gallons): $V_F =$	15	@ 10.00 MIN
AVERAGE FLOW RATE (GPM) =	1.50	
"STABILIZED" FLOW RATE (CFS): $Q =$	3.3E-03	
HYDRAULIC CONDUCTIVITY (CFS / FT² - FT. HEAD): $K =$	2.1E-04	



Soil Profile	
Depth (in-bls)	Description
0 - 48	Gray fine sand (SP)
48 - 72	Light brown fine sand (SP)
Groundwater encountered @ 24" below grade	

NOTES:
 The hydraulic conductivity test was performed in general accordance with the methods described in the South Florida Water Management District (SFWMD) Environmental Resource Permit Information Manual (Volume IV).
 The K-value was calculated based on the exfiltration test procedure as shown hereon.
 The presented hydraulic conductivity (K) value is applicable for an exfiltration trench installed at the same depth as the borehole test. The K-value represents an ultimate value. The designer should decide on the required factor of safety (minimum of 2, per SFWMD).

APPENDIX IV

AACE Project Limitations and Conditions

ANDERSEN ANDRE CONSULTING ENGINEERS, INC.

Project Limitations and Conditions

Andersen Andre Consulting Engineers, Inc. has prepared this report for our client for his exclusive use, in accordance with generally accepted soil and foundation engineering practices. No other warranty, expressed or implied, is made herein. Further, the report, in all cases, is subject to the following limitations and conditions:

VARIABLE/UNANTICIPATED SUBSURFACE CONDITIONS

The engineering analysis, evaluation and subsequent recommendations presented herein are based on the data obtained from our field explorations, at the specific locations explored on the dates indicated in the report. This report does not reflect any subsurface variations (e.g. soil types, groundwater levels, etc.) which may occur adjacent or between borings.

The nature and extent of any such variations may not become evident until construction/excavation commences. In the event such variations are encountered, Andersen Andre Consulting Engineers, Inc. may find it necessary to (1) perform additional subsurface explorations, (2) conduct in-the-field observations of encountered variations, and/or re-evaluate the conclusions and recommendations presented herein.

We at Andersen Andre Consulting Engineers, Inc. recommend that the project specifications necessitate the contractor immediately notifying Andersen Andre Consulting Engineers, Inc., the owner and the design engineer (if applicable) if subsurface conditions are encountered that are different from those presented in this report.

No claim by the contractor for any conditions differing from those expected in the plans and specifications, or presented in this report, should be allowed unless the contractor notifies the owner and Andersen Andre Consulting Engineers, Inc. of such differing site conditions. Additionally, we recommend that all foundation work and site improvements be observed by a Andersen Andre Consulting Engineers, Inc. representative.

SOIL STRATA CHANGES

Soil strata changes are indicated by a horizontal line on the soil boring profiles (boring logs) presented within this report. However, the actual strata change may be more gradual and indistinct. Where changes occur between soil samples, the locations of the changes must be estimated using the available information and may not be at the exact depth indicated.

SINKHOLE POTENTIAL

Unless specifically requested in writing, a subsurface exploration performed by Andersen Andre Consulting Engineers, Inc. is not intended to be an evaluation for sinkhole potential.

MISINTERPRETATION OF SUBSURFACE SOIL EXPLORATION REPORT

Andersen Andre Consulting Engineers, Inc. is responsible for the conclusions and recommendations presented herein, based upon the subsurface data obtained during this project. If others render conclusions or opinions, or make recommendations based upon the data presented in this report, those conclusions, opinions and/or recommendations are not the responsibility of Andersen Andre Consulting Engineers, Inc.

CHANGED STRUCTURE OR LOCATION

This report was prepared to assist the owner, architect and/or civil engineer in the design of the subject project. If any changes in the construction, design and/or location of the structures as discussed in this report are planned, or if any structures are included or added that are not discussed in this report, the conclusions and recommendations contained in this report may not be valid. All such changes in the project plans should be made known to Andersen Andre Consulting Engineers, Inc. for our subsequent re-evaluation.

USE OF REPORT BY BIDDERS

Bidders who are reviewing this report prior to submission of a bid are cautioned that this report was prepared to assist the owners and project designers. Bidders should coordinate their own subsurface explorations (e.g.; soil borings, test pits, etc.) for the purpose of determining any conditions that may affect construction operations. Andersen Andre Consulting Engineers, Inc. cannot be held responsible for any interpretations made using this report or the attached boring logs with regard to their adequacy in reflecting subsurface conditions which may affect construction operations.

IN-THE-FIELD OBSERVATIONS

Andersen Andre Consulting Engineers, Inc. attempts to identify subsurface conditions, including soil stratigraphy, water levels, zones of lost circulation, "hard" or "soft" drilling, subsurface obstructions, etc. However, lack of mention in the report does not preclude the presence of such conditions.

LOCATION OF BURIED OBJECTS

Users of this report are cautioned that there was no requirement for Andersen Andre Consulting Engineers, Inc. to attempt to locate any man-made, underground objects during the course of this exploration, and that no attempts to locate any such objects were performed. Andersen Andre Consulting Engineers, Inc. cannot be responsible for any buried man-made objects which are subsequently encountered during construction.

PASSAGE OF TIME

This report reflects subsurface conditions that were encountered at the time/date indicated in the report. Significant changes can occur at the site during the passage of time. The user of the report recognizes the inherent risk in using the information presented herein after a reasonable amount of time has passed. We recommend the user of the report contact Andersen Andre Consulting Engineers, Inc. with any questions or concerns regarding this issue.

Important Information about Your Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared *solely* for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. *And no one — not even you — should apply the report for any purpose or project except the one originally contemplated.*

Read the Full Report

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

A Geotechnical Engineering Report Is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- not prepared for your project,
- not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are *Not* Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.*

A Geotechnical Engineering Report Is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineering report. Reduce that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure contractors have sufficient time* to perform additional study. Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform a *geoenvironmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the *express purpose* of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; ***none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.***

Rely, on Your ASFE-Member Geotechnical Engineer for Additional Assistance

Membership in ASFE/THE BEST PEOPLE ON EARTH exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your ASFE-member geotechnical engineer for more information.

ASFE THE GEOPROFESSIONAL BUSINESS ASSOCIATION

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